# SOFTWARE BASED ANALYSIS, DESIGN AND MODELING OF A MULTISTORY BUILDING



## FINAL YEAR PROJECT UG 2017

## BY

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## Certification

This is to certify that the Thesis titled

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Submitted by

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has been accepted towards the fulfillment of the requirements

For Bachelor's in Civil Engineering

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### DEDICATED

## ТО

## OUR BELOVED PARENTS

# FOR THEIR UNWAVERING SUPPORT AND ENCOURAGEMENT

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### 1. Abstract

Analysis design and modeling of a multistory structure is a design-oriented project. The aim of this project was Structural design and detailing of multi-story residential/commercial building using essential civil engineering software. The First software used was AUTOCAD. It was used to have a layout of the building including all the architectural maps and all the components of building which were to be assigned. ETABs was used for the analysis and design of the building. First the grid was assigned and then all the components were defined. The live load and dead load was calculated and then all the components were assigned. Finally analysis and design was done and the loads were collected which then were to be applied on the foundation for its design. The codes (name of codes) were used as a reference material for design. All the detailing was done using CSI details and finally the foundation was designed using CSI SAFE.

### ACKNOWLEDGEMENTS

We are thankful to ALLAH ALMIGHTY for all his blessings and bestowing us with the strength and skills necessary for the task. We would like to show gratitude to Sir Ather Ali for providing us with the opportunity to perform this project and guide us in the completion of the project. We would like to thank our Head of CIVIL Department of SCEE and Principal of NICE whose support has been crucial to us for the completion of our venture. We would like to thank our teachers who helped us with dedication and commitment at NUST. We would also like to acknowledge the support of the Department of Civil Engineering for providing us adequate resources and work space within the premises of university to accomplish our task efficiently. We are also grateful to our families who have supported us morally and financially at every step. Last but not the least I would like to thank my friends especially M.Shazeb Khan and Uzair Azhar for their unconditional support during the tenure of our degree.

## 2. Introduction

The purpose of this project is to use our civil engineering knowledge and apply it by learning different civil engineering software like ETABS, SAFE, AUTOCAD, REVIT and 3Ds max and using them to create an economical and industry level design with complete structural drawings of a multistory building. This project will help us be familiarized with all the codes which were used during this project to get us ready for industrial level design. Using all the software we have all the design steps required to perfect a multistory building design.

### 3. Background

To select our multi story building we searched for a building which has a higher level of complexity compared to usual multistory residential building. After some research we selected Kaur Complex for our project which is in Peshawar, KPK. Kaur Complex is a dedicated project for families living in Peshawar which provides a secured gated community with 600+ apartments in total exclusively state of the art international standard apartments and condominiums, shops, and luxury penthouses. This multistory building was recently built, and it contains components like Residential and commercial area within the same floor, Elevators, Penthouse containing swimming pools, Water tank and basements. We referred to building codes for our design consideration. We started our project using ETABS. ETABS is the revolutionary ultimate integrated software package used to analyze and design structure. It can be used to design buildings of 1 story up to a skyscraper with variable level of complexity. It was developed by Computers and Structures, Inc. This software was used for analysis and design of our multistory building considering all the components in the design. Using the data from our design from ETABS, we use the software SAFE for our foundation design. SAFE is the ultimate tool for designing concrete floor and foundation systems. From framing layout to detail drawing production, SAFE integrates every aspect of the engineering design process in one easy and intuitive environment. SAFE provides unmatched productivity to the engineer with its truly unique combination of power, comprehensive capabilities, and ease-of-use. Laying out models is quick and efficient with the sophisticated drawing tools or uses one of the import options to bring in data from CAD, spreadsheet, or database programs. Slabs or foundations can be of any shape and can include edges shaped with circular and spline curves. Models can have columns, braces, walls, and ramps connected from the floors above and below. Walls can be modeled as either straight or curved.

# 4. Methodology:

#### **AUTOCAD:**

For Kaur complex we have drawings for each floor including all the details and components. All the dimensions required are in the drawings. We have 2 basements which are used for underground parking. The ramp starts from ground floor and goes to lower basement. Ground floor and the First floor houses residential and commercial area. About 50% area is commercial and 50% is residential divided by a wall. From 2<sup>nd</sup> floor till 9<sup>th</sup> floor, the area is residential and on the 9<sup>th</sup> floor there is a penthouse containing swimming pools and other luxuries. The roof contains Overhead Water tank. The building includes Elevators and stairs. All these components are to be accounted for in design.

#### **ETABS:**

First, we will be initializing model and define codes we will be using. The codes used were (ACI 3.18-14

#### 1. Defining Grid and Story Data:

By using architectural plan, we have defined grid. And we have assigned all the floors which were taken from architectural plans. The height of basement is 10.75 and rest of the floors are 11.75. The Elevations are assigned and -5ft is taken for foundation under basement and the rest of the elevations are according to the floor heights.

#### 2. Defining material:

We have defined 4 types of materials. These were Concrete Fc 4000psi, Concrete Fc 3000psi, Steel Gr60, Steel Gr50 for walls we have assigned Masonry of 3000psi. All these materials were assigned as we are using hit and trial method and we will be taking the material accordingly. We modify our material property. The properties of material are selected by ETABS automatically and Unit weight of concrete is takes as 150 lb./ft<sup>2</sup> and the unit weight of Steel is taken as 480 lb/ft<sup>2</sup>.

#### 3. Defining Columns:

We have given 3 types of columns. Outside Columns are taken as 30"x30". For interior columns we have selected circular columns for aesthetic purpose with 30" diameter. We use 4000 psi concrete. We modify our stiffness value using ACI 318-19, the moment of inertia taken is of 0.7Ig as they are weak in tension than in compression. Then we modify our rebar. Referring to the code we have selected 1.5" cover and we change reinforcement configuration as rectangular and circular accordingly.

#### 4. **Defining Beams**:

We have selected rectangular beam of  $12^{\circ}x20^{\circ}$ . Again, we changed our stiffness modifiers using ACI 319-19 we selected moment of inertia to be 0.35Ig. The Beam was assumed to be unsuitable for torsion, so the value was assigned a factor of 0.01. The cover given was of 2" for both top and bottom bars.

#### 5. Defining Slab:

We selected a 6" shell thin slab as we assume shear stresses to be 0. The stiffness modifiers are taken from the code. Modifying stiffness modifiers from ACI 318-19 we took moment of inertia to be 0.25Ig.

#### 6. Defining Loads:

First, we assigned our load patterns. ETABS calculates Dead load by itself, so the multiplier is 1. Then we have calculated super imposed deal load. All the loads are accommodated including Floor load was taken as 36psf, masonry wall of 9" as 990 psf. Masonry Wall of 4.5" as 445 psf and Concrete wall of 6" as 825 psf. For live load all the live loads ae taken from the code ASCE 7-16 (Enter code table).

After defining all the components, we assigned all the components on the ETABS.

#### 7. Assigning Frames:

In frame we have all the beams and columns. First, we placed our columns using (enter Command). We have all the gridlines we need to map our columns accordingly placing rectangular corner columns and circular columns interior columns. Then we placed our beams between our columns using (enter command).

#### 8. Assigning Slabs:

After setting up our frame we place our slabs on our frames. For trial we have taken slabs of a 6". The opening is left for elevator which follows from basement to last floor. We have left one slab of 7" on roof for support of elevator connection.

#### 9. Assigning Elevator walls:

Walls of Elevators were created using (enter command). We enter all the dimensions required to create shear walls. There is one passenger lift and one cargo lift.

#### **10.** Assigning staircase:

We have added Landing of the staircase in the form of a resting slab by introducing a reference plane to add a slab in between 2 floors. Next, mini ramps were added from one landing to another.

#### **Assigning load**

In assigning the loads the load was applied on slabs, Live load and superimposed dead load of floor finishes was applied on slabs, and load of walls was applied on beams manually while the dead load calculation of all members was done by CSI Etabs itself. Those labs which lie in a residential part of the building, the residential live load was applied on those buildings, similarly, those slabs which lie in the commercial part of the building live load was applied on them accordingly. Transference of load from slabs to beam and beams to the column was done by Etabs.

#### Analysis

Then analysis of the building was performed by CSI Etabs, in analysis of the building Etabs produced the SFD and BMD of the members of the building and calculated the forces that were being applied to the building and the reactions which were resisting the loading. In this way, all the applied loadings and reactions were obtained.

#### Design

In the design phase, the first stage frames were designed i.e., beams and columns on the Etabs. And in the results, Etabs produced the rebar percentage of top and bottom bars separately of beams.

Similarly, the design of columns which was done by the Etabs obtained the amount of steel needed in columns.

After the design of the frames, the design of the slab was started and performed by the Etabs, the rebar percentage needed for the slab was obtained, and then the design of the shear wall was also performed on Etabs.

#### **Design of Retaining wall**

Retaining wall cannot be designed in Etabs, retaining wall was designed manually on excel sheet considering all the parameters of design, to verify the design all the checks were applied on the designed retaining wall, all the checks were passed indicating that design was appropriate.

#### SAFE SOFTWARE PART

Results of analysis produced by Etabs were imported into this software and the design of the foundation was started. The material for the foundation was defined in software for designing purpose which includes the strength of concrete in terms of Psi, grade of steel, and then the slab for the foundation which is raft foundation was defined to the software. We initially started with a small thickness of slab of raft foundation and kept on increasing the thickness/depth until the design was satisfied, and then applied both the checks required for foundation design which were settlement check and bearing capacity check and punching shear check all of which were satisfied against the design, while the allowable settlement that was 50mm from ACI-318 and the building capacity of soil that is 1800 lb/ft<sup>2</sup> and the factor of safety equal to 3 was known from the soil profile. The punching shear check was the problem because the foundation was failing in punching shear again and again, to overcome this failure, the depth of the foundation was increased and extended with an offset a bit more than the outer line of the column. And the punching shear value for all the columns was less than 1, the check was passed. SAFE software generated the results for a foundation giving the results in in2/ft.

#### Detailing

After the designing phase detailing of the members was performed, detailing of each slab column beam elevator and the foundation present in the building was prepared by the software. In the detailing generated by the software, the number of bars used as reinforcement and the number of bars used as stirrups along with the spacing required for each member on each floor were obtained. As the floor changed, the loads on each member was also changed so the design and software-generated detailing of each member was obtained according to its load applied and members capacity to bear it. This means the software did not design all the members for the same load.

#### **Excel sheets**

Design excel sheets were also prepared.

- Retaining Wall
- Slabs

All the ACI checks were also applied on those manually designed members, to counter verify the pertinence of design.

# 5. Results.

### > Column





#### **Complete Detailing of one column**





As we can see there are A, B, C, D,E,F and G sections in which detailing, and dimension of our column is different.







Figure 4

### > Beams

### **Beam Framing Plan**



Figure 5

#### **Typical Concrete Beam Elevation**





Figure 6



### **Complete Detailing of one beam**



Figure 9





#### **Detailing of sections**





Figure 11

### > Slab

We Designed slab by using strip-based Method.

#### Floor framing plan of a typical floor.



Figure 13

### **Close Detailing of one Section**

### 1) Slab Top Rebar Plan



### 2) Bottom Rebar plan





#### 3) Slab Total Rebar plan





### > Elevator



#### **Detailing of Single Section**

Figure 18











Figure 21

✓ Passed

### **Final Rebar Plan of Raft**



Figure 22

| 6. | Design | <b>Sheet for</b> | Retaining | Wall |
|----|--------|------------------|-----------|------|
|    |        |                  |           |      |

|       | In                               | put Data       |      |  |  |
|-------|----------------------------------|----------------|------|--|--|
| Sr.No | f <sub>c</sub>                   | 4              | ksi  |  |  |
|       | f <sub>y</sub>                   | 60             | ksi  |  |  |
|       | h                                | 26.5           | ft   |  |  |
|       | W <sub>s</sub>                   | 130            | pcf  |  |  |
|       | Wc                               | 150            | pcf  |  |  |
|       | W <sub>w</sub>                   | 62.4           | pcf  |  |  |
|       | Surcharge Load                   | 200            | psf  |  |  |
|       | Cover                            | 1.5            | in   |  |  |
|       | d <sub>b</sub>                   | 0.5            | in   |  |  |
|       | L                                | 26.25          | ft   |  |  |
|       | Lateral I                        | Earth Pressure |      |  |  |
|       | C <sub>a</sub>                   | 0              |      |  |  |
|       | $P_a = Ca\omega h$               | 0              | ksf  |  |  |
|       | $H_a = 1/2 P_a h$                | 0              | K/ft |  |  |
|       | Fram Base, H <sub>a</sub> acts @ | 8.8333         | ft   |  |  |
|       | Surch                            | narge Load     |      |  |  |
|       | Surcharge Height, h <sub>s</sub> | 1.54           | ft   |  |  |
|       | $P_s = Ca\omega h_s$             | 0              | ksf  |  |  |
|       | $H_s = P_s h$                    | 0              | K/ft |  |  |
|       | Fram Base, H <sub>a</sub> acts @ | 13.25          | ft   |  |  |
|       |                                  |                |      |  |  |
|       |                                  |                |      |  |  |
|       | Lateral                          | Water Pres     | sure |  |  |

|                             | Lateral Water Pressure                         |             |             |  |  |  |  |  |  |  |
|-----------------------------|--|-------------|-------------|--|--|--|--|--|--|--|
|                             | C <sub>a</sub>                                 | 1           |             |  |  |  |  |  |  |  |
|                             | $P_w = Ca\omega h$                             | 1.6536      | ksf         |  |  |  |  |  |  |  |
|                             | $H_w = 1/2 P_w h$                              | 21.9102     | K/ft        |  |  |  |  |  |  |  |
|                             | H'w=Hw/2                                       | 10.9551     | K/ft        |  |  |  |  |  |  |  |
|                             | Fram Base, H <sup>'</sup> <sub>w</sub> acts @  | 8.833       | ft          |  |  |  |  |  |  |  |
|                             | Factored Loads                                 |             |             |  |  |  |  |  |  |  |
|                             | 1.6H <sub>a</sub>                              | 0           | K/ft        |  |  |  |  |  |  |  |
|                             | 1.6H <sub>s</sub>                              | 0           | K/ft        |  |  |  |  |  |  |  |
|                             | 1.6H <sub>w</sub>                              | 35.05632    | K/ft        |  |  |  |  |  |  |  |
|                             | 1.6H <sup>'</sup> <sub>w</sub>                 | 17.52816    | K/ft        |  |  |  |  |  |  |  |
| Moments & Shears (Uniform L |  |             |             |  |  |  |  |  |  |  |
|                             | $M_{u(A)}$ due to Uniform Load                 | 0.0000      | K-ft        |  |  |  |  |  |  |  |
|                             | M <sub>u(C)</sub> due to Uniform Load          | 0           | K-ft        |  |  |  |  |  |  |  |
|                             | Maximum Positive M <sub>c</sub> from Base is @ | 9.9375      | ft          |  |  |  |  |  |  |  |
|                             | m=x/L, x=3L/8                                  | 0.375       | ft          |  |  |  |  |  |  |  |
|                             | $\Delta_{\rm x}$                               |             |             |  |  |  |  |  |  |  |
|                             | $\Delta_{ m max}$                              |             |             |  |  |  |  |  |  |  |
|                             | Moments & She                                  | ars (Triang | gular Load) |  |  |  |  |  |  |  |
|                             | $M_{u(A)}$ due to Triangular Load              | 61.349      |             |  |  |  |  |  |  |  |
|                             | M <sub>u(C)</sub> due to Triangular Load       | 2.103       |             |  |  |  |  |  |  |  |
|                             | Maximum Positive $M_c$ from Base is @          |             |             |  |  |  |  |  |  |  |
|                             | R  | eactions    |             |  |  |  |  |  |  |  |
|                             | $R_A = V_A$                                    | 14.023      | Kips        |  |  |  |  |  |  |  |
|                             | $R_B = V_B$                                    | 3.505632    | Kips        |  |  |  |  |  |  |  |

| -  |  |   |
|--|--|---|
| Analysis & Design  | n for Negat  | ive Moment  |
| Steel %age =   | 1  | %   |
| R <sub>u</sub>   | 443  | psi   |
| Effective Depth=d  | 11.768   | in  |
| Total Depth=h=d+cover+d <sub>b</sub> /2  | 13.518   |   |
| Depth used=h   | 7.5  | in  |
| Effective Depth=d  | 5.75   |   |
| Ru   | 1856   | psi   |
| Steel Ratio=   | 0.0054   |   |
| Steel Area=A <sub>s</sub>  | 0.3726   | in <sup>2</sup>   |
| Minimum Steel=A <sub>s,min</sub>   | 0.135  | in <sup>2</sup>   |
| Steel for Flexure=A <sub>s,f</sub>   | 0.2277   | in <sup>2</sup>   |
| Steel Used=  | 0.3726   | in <sup>2</sup>   |
| Steel Bar  | 4  | #   |
| Area of Bar=A <sub>b</sub>   | 0.20   | in <sup>2</sup>   |
| Spacing=S  | 6 32365671   | in  |
| spacing s  | 0.52505071   | 111   |
| Analysis & Desig   | n for Positi   | ve Moment   |
| Analysis & Desig   | n for Positi<br>504.506059   | <b>ive Moment</b><br>psi  |
| Analysis & Desig<br>Ru<br>Steel Ratio=   | n for Positi<br>504.506059<br>0.002  | ive Moment<br>psi   |
| Analysis & Desig Ru Steel Ratio= Steel Area=A <sub>s</sub>   | n for Positi<br>504.506059<br>0.002<br>0.14  | in psi<br>in <sup>2</sup>   |
| Analysis & Desig       Ru       Steel Ratio=       Steel Area=A <sub>s</sub> Steel for Flexure=A <sub>s,f</sub>  | n for Positi<br>504.506059<br>0.002<br>0.14<br>0.23  | ive Moment<br>psi<br>in <sup>2</sup><br>in <sup>2</sup>   |
| Analysis & Desig       Ru       Steel Ratio=       Steel Area=As       Steel for Flexure=As,       Steel Used=   | n for Positi<br>504.506059<br>0.002<br>0.14<br>0.23<br>0.23  | in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup>   |
| Analysis & Desig         Ru         Steel Ratio=         Steel Area=As         Steel for Flexure=As,f         Steel Used=         Steel Bar  | n for Positi<br>504.506059<br>0.002<br>0.14<br>0.23<br>0.23<br>4   | in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup><br>#   |
| Analysis & Desig       Ru       Steel Ratio=       Steel Area= $A_s$ Steel for Flexure= $A_{s,f}$ Steel Used=       Steel Bar       Area of Bar= $A_b$   | n for Positi<br>504.506059<br>0.002<br>0.14<br>0.23<br>0.23<br>4<br>0.20   | in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup><br>#<br>in <sup>2</sup>  |
| Analysis & Desig         Analysis & Desig         Ru       Steel Ratio=         Steel Ratio=       Steel Area=A_s         Steel for Flexure=A_s, f       Steel Used=         Steel Bar       Area of Bar=A_b         Spacing=S       Steel S | n for Positi<br>504.506059<br>0.002<br>0.14<br>0.23<br>0.23<br>4<br>0.20<br>10.3478019   | in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup>   |
| Analysis & Desig         Analysis & Desig         Ru       Steel Ratio=         Steel Ratio=       Steel Area= $A_s$ Steel for Flexure= $A_{s,f}$ Steel Used=         Steel Bar       Area of Bar= $A_b$ Spacing=S       Longitudin  | n for Positi<br>504.506059<br>0.002<br>0.14<br>0.23<br>0.23<br>4<br>0.20<br>10.3478019<br>al Reinfoce  | in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup><br>#<br>in <sup>2</sup><br>in<br>ement   |
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| Analysis & Desig         Ru         Steel Ratio=         Steel Area= $A_s$ Steel for Flexure= $A_{s,f}$ Steel Used=         Steel Bar         Area of Bar= $A_b$ Spacing=S         Longitudin         Steel Ratio=         Steel Area= $A_s$   | n for Positi<br>504.506059<br>0.002<br>0.14<br>0.23<br>0.23<br>4<br>0.20<br>10.3478019<br>al Reinfocc<br>0.002<br>0.18                       | in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup><br>in<br>ement<br>in <sup>2</sup>   |
| Analysis & Desig         Analysis & Desig         Ru       Steel Ratio=         Steel Area= $A_s$ Steel for Flexure= $A_{s,f}$ Steel Iosed=       Steel Bar         Area of Bar= $A_b$ Spacing= $S$ Longitudin         Steel Ratio=       Steel Area= $A_s$ Steel Bar       Steel Ratio=         Steel Bar       Steel Area= $A_s$ Steel Bar       Steel Bar   | n for Positi<br>504.506059<br>0.002<br>0.14<br>0.23<br>0.23<br>4<br>0.20<br>10.3478019<br>al Reinfoce<br>0.002<br>0.18<br>4                  | in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup><br>#<br>in <sup>2</sup><br>in<br>ement<br>in <sup>2</sup><br>in<br>ement   |
| Analysis & Desig         Analysis & Desig         Ru       Steel Ratio=         Steel Ratio=       Steel Area= $A_s$ Steel Isar       Area of Bar= $A_b$ Spacing=S       Longitudin         Steel Area= $A_s$ Steel Ratio=         Steel Bar       Area of Bar= $A_b$ Steel Ratio=       Steel Bar         Area of Bar= $A_b$ Steel Bar         Area of Bar= $A_b$ Steel Bar   | n for Positi<br>504.506059<br>0.002<br>0.14<br>0.23<br>0.23<br>4<br>0.20<br>10.3478019<br>al Reinfocc<br>0.002<br>0.18<br>4<br>0.20          | in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup><br>in<br>ement<br>in <sup>2</sup><br>in<br>ement<br>in <sup>2</sup><br>in<br>ement<br>in <sup>2</sup>                               |
| Analysis & Desig         Analysis & Desig         Ru       Steel Ratio=         Steel Area= $A_s$ Steel for Flexure= $A_{s,f}$ Steel Iosed=       Steel Bar         Area of Bar= $A_b$ Spacing=S         Longitudin         Steel Ratio=       Steel Area= $A_s$ Steel Bar       Area of Bar= $A_b$ Steel Bar       Area of Bar= $A_b$ Steel Bar       Area of Bar= $A_b$ Steel Sar       Steel Bar         Area of Bar= $A_b$ Spacing=S   | n for Positi<br>504.506059<br>0.002<br>0.14<br>0.23<br>0.23<br>4<br>0.20<br>10.3478019<br>al Reinfocc<br>0.002<br>0.18<br>4<br>0.20<br>13.09 | in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup><br>in <sup>2</sup><br>#<br>in <sup>2</sup><br>in<br>ement<br>in <sup>2</sup><br>in<br>ement<br>in <sup>2</sup><br>in <sup>2</sup><br>in<br>in<br>ement<br>in <sup>2</sup> |

# 7. Design Sheet for Slab

|    |                              | <u> </u>        |         |                         |            |            |              |              |             |              |            |              |              |          |
|----|------------------------------|-----------------|---------|-------------------------|------------|------------|--------------|--------------|-------------|--------------|------------|--------------|--------------|----------|
|    | A                            | В               | С       | D                       | E          | F          | G            | Н            | I           | J            | K          | L            | М            | N        |
| 1  |                              |                 |         |                         |            |            |              |              |             |              |            |              |              |          |
| 2  | Design of Slab               |                 |         |                         |            |            |              |              |             |              |            |              |              |          |
| 3  |                              |                 |         |                         |            |            |              |              |             |              |            |              |              |          |
| 4  |                              |                 |         |                         |            |            |              |              |             |              |            |              |              |          |
| 5  |                              |                 |         |                         |            |            |              |              |             |              |            |              |              |          |
| 6  |                              |                 |         |                         |            |            |              |              |             |              |            |              |              |          |
| 7  |                              |                 |         |                         |            |            |              |              |             |              |            |              |              |          |
| 8  | INPUT DATA:                  |                 |         |                         |            |            |              |              |             |              |            |              |              |          |
| 9  |                              |                 |         |                         |            |            |              |              |             |              |            |              |              |          |
| 10 | SLAB DIN                     | <b>IESNIONS</b> |         |                         |            |            |              |              |             |              |            |              |              |          |
| 11 |                              |                 |         |                         |            |            |              |              |             |              |            |              |              |          |
| 12 | Short spar                   | ้า              |         | lx                      | 20         | feet       |              |              |             |              |            |              |              |          |
| 13 | Long span                    |                 |         | ly                      | 25         | feet       |              |              |             |              |            |              |              |          |
| 14 | Aspect rat                   | io              |         | m                       | 0.8        |            |              |              |             |              |            |              |              |          |
| 15 | Thickness                    | of slab (Mir    | nimum ) | h(min)                  | 6          | inch       | If your slat | s is support | ed on all 4 | sides throu  | gh beams h | n should not | be less that | n 5 inch |
| 16 | Thickness                    | of slab (pro    | vided)  | h                       | 6          | inch       | ACI 9.5.3.2  | 2            |             |              |            |              |              |          |
| 17 |                              |                 |         |                         |            |            | SLAB WITH    | HOUT DROP    | PANEL H r   | nin = 5 incl | า          |              |              |          |
| 18 |                              |                 |         | da                      | 5          | inch       | SLAB WITH    | I DROP PAN   | NEL H min = | 4 inch       |            |              |              |          |
| 19 |                              |                 |         | db                      | 4.5        | inch       |              |              |             |              |            |              |              |          |
| 20 |                              |                 |         |                         |            |            |              |              |             |              |            |              |              |          |
| 21 | END CONI                     | DTIONS          |         |                         |            |            |              |              |             |              |            |              |              |          |
| 22 | Shoter spa                   | an end conf     | ition   | <mark>one edge c</mark> | onti and o | ne discont | i            |              |             |              |            |              |              |          |
| 23 | 23 longer span end condition |                 |         | one edge c              | onti and o | ne discont | i            |              |             |              |            |              |              |          |

| 24 | coefficeint for shorter span         |            |       |
|----|--------------------------------------|------------|-------|
| 25 | coefficient of dead positive moments | Ca(+)D.L   | 0.039 |
| 26 | coefficient of live positive moments | Ca(+)L.L   | 0.048 |
| 27 | coefficient of negative moments      | Ca(-)DL+LL | 0.071 |
| 28 |                                      |            |       |
| 29 |                                      |            |       |
| 30 | coefficeint for longer span          |            |       |
| 31 | coefficient of dead positive moments | Cb(+)D.L   | 0.016 |
| 32 | coefficient of live positive moments | Cb(+)L.L   | 0.02  |
| 33 | coefficient of negative moments      | Cb(-)DL+LL | 0.029 |
| 34 |                                      |            |       |

| 35 | APPLIED LOADING         |         |       |         |
|----|-------------------------|---------|-------|---------|
| 36 | Self weight             | 75      | psf   |         |
| 37 | Service Dead Load       | 100     |       |         |
| 38 | Service Live Load       | 100     |       |         |
| 39 |                         |         |       |         |
| 40 | Load of water           |         |       |         |
| 41 | unit weight of water    |         | 62.43 | lb/ft^3 |
| 42 | Height of pool or tank  | c       | 0     | ft      |
| 43 | Total weight of water   | 0       | psf   |         |
| 44 | For pool additional liv | e load  | 10    | psf     |
| 45 |                         |         |       |         |
| 46 | ultimate load of pool   |         | 16    |         |
| 47 | Total actual load       |         |       |         |
| 48 | factored dead load      |         | 210   | psf     |
| 49 | factored live load      |         | 176   | psf     |
| 50 | Total ultimate Factore  | ed load | 386   | psf     |
| 51 |                         |         |       |         |

| 52 | MATERIAL    | STRENGT      | H            |             |      |         |       |
|----|-------------|--------------|--------------|-------------|------|---------|-------|
| 53 | Concrete    | fc           | 3            |             |      |         |       |
| 54 | steel       | fy           | 60           |             |      |         |       |
| 55 |             |              |              |             |      |         |       |
| 56 |             |              |              |             |      |         |       |
| 57 | LOA         | ADS .        |              |             |      |         |       |
| 58 | Total ult   | imate DL     | WD.L         |             | 210  |         |       |
| 59 | Total ult   | imate LL     | WL.L         |             | 176  |         |       |
| 60 | Total ultim | nate Factor  | ed load      | Wu          | 386  |         |       |
| 61 |             |              |              |             |      |         |       |
| 62 | DES         | IGN MOM      | ENTS         |             |      |         |       |
| 63 | M(-ve) in s | horter spa   | n DL+LL      |             |      | 10962.4 | lb-ft |
| 64 | M(-ve) in I | onger span   | at DL+LL in  | terior supp | orts | 6996.25 | lb-ft |
| 65 | M(+ve) DL   | in shorter   | span at mid  | span        |      | 3276    | lb-ft |
| 66 | M(+ve) DL   | in longer s  | pan at mid   | span        |      | 2100    | lb-ft |
| 67 | M(+ve) LL   | in shorter s | span at mid  | span        |      | 3379.2  | lb-ft |
| 68 | M(+ve) LL   | in longer sj | oan at mid s | span        |      | 2200    | lb-ft |
| 69 | M(-ve) in s | horter spa   | n at Discon  | tinues edge |      | 2218.4  | lb-ft |
| 70 | M(-ve) in I | onger span   | at Disconti  | nues edge   |      | 1433.33 | lb-ft |

| 73 |   |              |              |             |      |           |          |         |      |
|----|---|--------------|--------------|-------------|------|-----------|----------|---------|------|
| 74 | M(-ve) in s                                   | horter spar  | n DL+LL      |             |      | 10962.4   | lb-ft    | 10.9624 | k-ft |
| 75 | M(-ve) in l                                   | onger span   | at DL+LL in  | terior supp | orts | 6996.25   | lb-ft    | 6.99625 | k-ft |
| 76 | TOTAL M(+                                     | +ve) in shoi | rter span af | t mid span  |      | 6655.2    | lb-ft    | 6.6552  | k-ft |
| 77 | TOTAL M(-                                     | +ve) in long | ger span at  | mid span    |      | 4300      | lb-ft    | 4.3     | k-ft |
| 78 | M(-ve) in s                                   | horter spar  | n at Discon  | tinues edge |      | 5872.53   | lb-ft    | 5.87253 | k-ft |
| 79 | M(-ve) in longer span at Discontinues edge    |              |              |             |      | 3765.42   | lb-ft    | 3.76542 | k-ft |
| 80 |   |              |              |             |      |           |          |         |      |
| 81 |   |              |              |             |      |           |          |         |      |
| 82 | AREA OF S                                     | TEEL REQU    | IIRED        |             |      | Ast = Mu/ | fy(0.9d) |         |      |
| 83 | for M(-ve)                                    | in shorter s | span interio | or          |      | Ast       | 0.48722  | in^2    |      |
| 84 | for M(-ve)                                    | in longer sp | oan at inter | ior         |      | Ast       | 0.34549  | in^2    |      |
| 85 | for M(+ve)                                    | in shorter   | span at mic  | dspan       |      | Ast       | 0.29579  | in^2    |      |
| 86 | for M(+ve)                                    | in longer s  | pan at mid   | span        |      | Ast       | 0.21235  | in^2    |      |
| 87 | for M(-ve)                                    | in shorter s | span at Disc | continues e | dge  | Ast       | 0.261    | in^2    |      |
| 88 | for M(-ve) in longer span at Discontinues edg |              |              |             | ge   | Ast       | 0.18595  | in^2    |      |
| 89 |   |              |              |             |      |           |          |         |      |
| 90 |   |              |              |             |      |           |          |         |      |

| 94  |            |                        |                 |          |            |             |                                |                                |          |
|-----|------------|------------------------|-----------------|----------|------------|-------------|--------------------------------|--------------------------------|----------|
| 95  |            | number of bar selected |                 | #        | 3          |             | area of selected number of bar | 0.110447                       |          |
| 96  | in^2       |                        |                 |          |            |             |                                |                                |          |
| 97  | in^2       | Spacing                | S               | 3.398365 | inch       | c/c         |                                |                                |          |
| 98  |            |                        |                 |          |            |             |                                |                                |          |
| 99  | ERIOR      |                        |                 |          |            |             |                                |                                |          |
| 100 |            | number o               | of bar selec    | ted      | #          | 3           |                                | area of selected number of bar | 0.110447 |
| 101 | in^2       |                        |                 |          |            |             |                                |                                |          |
| 102 | in^3       | Spacing                | S               | 2.720267 | inch       | c/c         |                                |                                |          |
| 103 |            |                        |                 |          |            |             |                                |                                |          |
| 104 | CONTI      |                        |                 |          |            |             |                                |                                |          |
| 105 |            | number o               | of bar selec    | ted      | #          | 3           |                                | area of selected number of bar | 0.110447 |
| 106 |            |                        |                 |          |            |             |                                |                                |          |
| 107 |            | Spacing                | S               | 12       | inch       | c/c         |                                |                                |          |
| 108 |            |                        |                 |          |            |             |                                |                                |          |
| 109 | ONG LON    | GER SPAN               |                 |          |            |             |                                |                                |          |
| 110 |            |                        |                 |          |            |             |                                |                                |          |
| 111 |            | number o               | of bar selec    | ted      | #          | 3           |                                | area of selected number of bar | 0.110447 |
| 112 |            |                        |                 |          |            |             |                                |                                |          |
| 113 |            | Spacing                | S               | 6.241533 | inch       | c/c         |                                |                                |          |
| 114 |            |                        |                 |          |            |             |                                |                                |          |
| 115 | ERIOR      |                        |                 |          |            |             |                                |                                |          |
| 116 | 6 number o |                        | of bar selected |          | #          | 3           |                                | area of selected number of bar | 0.110447 |
| 117 |            |                        |                 |          |            |             |                                |                                |          |
| 118 |            | Spacing                | S               | 3.836139 | inch       | c/c         |                                |                                |          |
| 119 |            |                        |                 |          |            |             |                                |                                |          |
| 120 | CONTI      |                        |                 |          |            |             |                                |                                |          |
| 121 |            | number of bar selected |                 | #        | 3          |             | area of selected number of bar | 0.110447                       |          |
| 122 |            |                        |                 |          |            |             |                                |                                |          |
| 123 |            | Spacing                | S               | 12       | inch       | c/c         |                                |                                |          |
| 124 |            |                        |                 |          |            |             |                                |                                |          |
| 125 |            |                        |                 |          |            |             |                                |                                |          |
| 126 |            |                        |                 |          |            |             |                                |                                |          |
| 127 | nel        | =                      | 193             | kips     | Lx * Ly* W | Vu          |                                |                                |          |
| 128 |            |                        |                 |          |            |             |                                |                                |          |
| 129 | tion ΦVc   | =                      | 5.58677         | k/ft     | 0.85*2* (f | fc psi)^1/2 | * b*d/1000                     |                                |          |
| 130 | de Vua     | =                      | N.A             |          |            |             |                                |                                |          |
| 131 | le Vua     | =                      | 3.86            | k/ft     | (1*193)/   | (2*ly)      | <5.58677                       | ok                             |          |
|     | 1          |                        |                 |          |            |             |                                |                                |          |

## 8. Discussion:

The columns were designed by a hit and trial method. Nominal dimensions were selected, and the dimensions were increased until all the checks were passed. This way economical design was selected.

As for the beams, similar manual calculations were done to ensure and double check the accuracy of software calculations. The design was modified until all the checks were passed, final design and detailing was done.

Slabs were designed using stripped based method by software and to check the accuracy of software, manual calculations were done using design sheet of the slabs which conformed to the design of the slab using the software and ensures that all the checks were passed.

For the design of foundation, the dimensions were confirmed after making sure that punching shear check and bearing strength check were passed and finally the design of foundation was selected.

For the design of retaining wall, excel sheet was used. First, we analyzed the geotechnical soil site report and extracted all the necessary data of soil needed to be entered in the design sheet. According to our requirement we entered the steel percentage and all the required manual input to get all the data required and used it for the final design of retaining wall.

## 9. Conclusion:

With the help of Etabs software, design of all the members was conducted and all the checks were passed. Checks were performed by Etabs and manually as well. All the members passed the necessary ACI design checks. With this project, we got familiarized with the design procedure of a modern multistory building which included commercial and residential units inside the building. We also got familiarized with the Etabs software and we prepared manual design excel sheets of different structural elements of the building. In this project we learnt different parameters of the design which the software used.

# **10. References**

- ✓ https://www.csiamerica.com/products/etabs/videos
- ✓ https://www.csiamerica.com/products/safe/videos
- ✓ ACI 318-14
- ✓ ACI 318-18
- ✓ ASCE 7-10
- ✓ Design of Reinforced Concrete by Jack C. McCormack and Russell H