# Process Design and Simulation of Dimethyl Ether Production





# School of Chemical and Materials Engineering National University of Sciences and Technology 2022

# **Process Design and Simulation of Dimethyl**

# **Ether Production**



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MS in Process Systems Engineering Supervisor: Dr. Muhammad Ahsan School of Chemical and Materials Engineering (SCME) National University of Sciences and Technology (NUST) June 2022

### Declaration

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## Dedication

TO MY HONORED PARENTS, RESPECTED TEACHERS, AND ALL THOSE WHO DEDICATED THEIR YESTERDAY TO MY BLESSED TODAY

### Acknowledgement

Alhamdulillah, all praises to the **ALMIGHTY ALLAH** for his infinite blessings and strength in accomplishing this effort. All honour and respect are for his **HOLY PROPHET** (**PBUH**), whose teachings are a great source of wisdom and guidance for the entire human race.

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#### Abstract

The amount of energy we utilize has far-reaching consequences. For example, driving to work consumes fuel, which is ultimately tied to both foreign violence and global climate change. The ability to harness energy, particularly in the form of bio-fuels like oil, carbon, & natural gas, are crucial to the success of modern civilization. To satisfy this requirement and provide financial stability, renewable energy requirements are utilized as energy costs keep growing. For this reason, scientists in sustainable energy are working to make new tools and systems to reach their goals. Over the previous century, there has been a considerable overproduction of crude oil around the world. Consequently, natural gas has emerged as a potential substrate for the synthesis of minerals and energy in electricity and manufacturing. This substance can be utilized in various types of power generating, transportation fuel, and residential space heating. Through the use of synthesis gas, dimethyl ether is typically made as a precursor from fossil fuels, coal, and biomass. In recent times, the publicity to DME has expanded because of its willingness to remedy energy safeguards and global pollution. The first is an indirect method, in which the production and hydration of methanol are conducted to produce DME. Another technique is to synthesize DME directly from liquid fuels. In addition, to be used as substituted cobalt, it must be made in sufficient quantities at a reasonable cost. The aim of this research is to establish system syntheses, modelling, and integrating methodologies for a shale gas-to-DME plant using both, directly or indirectly, processes to achieve the desired results. A simulation model is also conducted to determine procedure sustainability under varying market situations. Finally, these systems are considered based on the fixed cost of capital, operation cost, financial returns and Carbon dioxide and the water impact. Alpine Plus carried out primary and secondary simulation software of a professional DME manufacturer to better understand how the factory operates. The feed for shale gas production was sourced by one of the reservoirs in the Denton shale play in the United States. The manufacturing capability of dimethyl ether in baseline conditions for explicit and implicit operations was estimated to be 3,250 tones per day.

It was possible to synthesize the internal and external process voidable contract by utilizing six and ten key processing phases, correspondingly. Squeeze research was employed in order to complete the heat incorporation of the system. After conducting a study, it was discovered that the aggressive route had a benefit over the indirect technique of permanent capital cost, operational costs (including maintenance costs), payout ratio, and the impact of CO2. The capital expenditure required for the sales derived technique is 20 percentage points less than the required for the analytical method. The direct approach is more cost-effective than that of the inductive channel from an economic perspective. When considering a susceptibility analysis, the costs of CH30H andshales gas are by far the important critical elements determining the developing

## Chapter 01

### **1** Introduction

#### 1.1 Natural Gas

The need for worldwide energies is continuously growing. The rise between 2009 and 2035 is estimated to be approximately 41 percent, following the International Energy Agency (Fig. 1-1). Therefore, to meet this demand and allow economic stability, renewable energy resources are required. The study continues to produce newer technologies and procedure's in lots of fields to achieve this objective[1, 2]. Behind the use of relevant resources of power, 82 percent of the energy needs of the United States are generated from resources [3].



Figure 1-1 Increasing resources expenditures around 2009 and 2035.

Among bio-fuels, the most extensive distribution is of natural gases. Evidence on the 2010 study by the multinational resources company, its share is almost twenty two % of the global supply of energy (Figure 1-2) Natural gas is consisted of methane butane, ethane, propane, and other gases. Methane, nevertheless, primary ingredient of the energy resources ,also proportion in typical constitution ranges around 80-95 percentage (Table 1-1). (Table 1-1). It is scent-free and colourless; its clean combustion makes it considerably more eco-sustainable than charcoal and oil [4, 5].



Figure 1-2 The concentration of various resources info supply

There are mountain ranges that produce natural gas; this type of gas is considered traditional and rare. Natural gas was primarily extracted from conventional sources until the last decade, but oil and gas extraction from nontraditional deposits has risen quickly in the latest generations. Due to its versatility, natural gas has lots of portions of use, such as manufacturing, locally and household. The more significant benefits of the other fossil fuels are their strength and clean-burning characteristics. In contrast with other fossil fuels, this makes it environmentally friendly. Natural gas restricts its significance in the upcoming projects of the energy world. In particular, due to its reliability characteristics, natural gas has a significant influence on the world economy. In the United States, 84 percent of natural gas is thus produced [6, 7].

Table 1-1 chemical compositions of natural gas	Table	1-1	chemical	compositions	of natural	gas
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Table 1: Chemical Composition of Conventional Natural Gas [8].

Components	Chemical Formula	Typical Com. (mol %)	Extreme (mol%)
Methane	CHDC	80 - 95	50-95
Ethane	DHDC	2-5	2 - 20
Propane	DHDC	1-3	1-12
Butane	OHOO	0-1	0 - 4
C5 alkanes and higher	C□+	0-1	0-1
hydrocarbon Carbon		No. 31-2	
Dioxide Nitrogen	COUN	1-5	0 - 99
HydrogenSulfide	DHDS	1-5	0 - 70
Oxygen	<b>O</b> □ Hetr	0-2	0-6
Helium	aces	0	0-0.2
Other inert gases		0 - 0.1	0-1

#### **1.2** What is Natural Gas?

Natural gas is known as standard as well as untraditional. One feature of untraditional natural gas is that it is contained in the mountains and the rocks with more availability—over 1000 micro-darts. Unusual natural gas, on the other hand, is found in rocks with a permeability of less than one millibar. The primary forms of unconventional natural gas are shale gas, tight gas, gas hydrates, and methane dependent on coal[6]. In shale deposits, shale gas is contained, and it is the resource material and reserve for natural gas. Compares favorably with other forms of fossil fuel, shale gas has the cleanest combustion and has the largest share in the upcoming resources strategy to supply energy needs [9].

More advanced technologies than traditional methods are needed for the manufacturing of gas from shale sources. However, over the last decade, the use of untraditional materials has been roaring quickly. Around 65 percent of natural gas, for instance, is extracted in North America from unconventional resources. This gas has the dominant effect on this progression among eccentricmeans[10].

The world has seen significant advances in the extraction of shale gas over the last decade. The first economic DME production was performed in Barents. (United States),currently more than 50,000 wells in about twenty regions. Shale gas manufacturing grew from 1 percent to twenty percent in ten years due to this revolution (2000 to 2010). This sum would increase by 46 percent by 2035.Fig. 1-4). The most significant impact of this revolution is less than \$6.00 per million of British thermal units (MMBTU) on the domestic gas price.



Figure 1-3 Indications of natural gas manufacturing depends on the alterative resources

## Chapter 02

## 2 Literature Review

#### 2.1 Dimethyl Ether Properties

DME is the lightest, completely danger free and does not contain any toxic elements as well as does not contain any C-C interactions, and the H/C proportion is high. It possesses physiological qualities comparable to those of LPG, and it allows DME to be stored and supplied with minimal change by utilizing current infrastructures and technologies. This is used as a substitute for LPG in cookery and thermal applications and an aerosols propulsion in acrylic paint and other aerosols productsThey can be manufactured from various materials of energy, oil, agricultural waste, bioenergy, trash and bio-fuel.

	Table 2-1	Physical	Properties	of DME
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Properties	DME	Methanol	Propane	Methane	Diesel fuel
Chemical	CH3OC	CH3O	C <sub>3</sub> H <sub>8</sub>	CH	
formula	H <sub>3</sub> 247.	H	231	4	180-
Boiling point	9	337.6	0.49	111	370
(K)	0.67	0.79	1.52	.5	0.84
Liquid density (g/cm3	1.59	2.0-0	426	-	-
at 293 K) Specific	467	1,0	9.3	0.5	-
are 200 it) opecifie	6.1	97	777	5	-
gravity (vs. air)	623	-	2.1-	510	84
Heat of vaporization	3.4-17	74	9.4	510	0.6-
(kJ/kg) Vapor pressure	55-60	3	01.05	00	6.5
(atm at 293 K)	59.44	55	91.25	50	40-
Ignition temperature	28.90	36	46.46	5	55
				5-15	-

Table 2 Physical properties of DME and other fuels [17].

In Table 2-1, the physical composition of the DME can be seen. DME's vapour pressure at 293 K is 6.1 atm, so it can quickly be liquefied with a minimal amount of pressure. As compared to propane, propane has identical physical characteristics. This feature makes it a blend to be used in LPG. Dimethyl ether has a higher clarifications value. Ratios are 1.38 and 1.66, comparatively. It explodes like gas. Dissolution of Dimethyl ether into the upper atmosphere somehow doesn't trigger greenhouse influence or ozone depletion deteriorating [17].

#### **2.2 DME Market**

Even though DME has a bright perspective, its quantity of implementation and advancement is still very modest around the globe. Between 1993 and 2012, on the other hand, there was significant growth in output potential. The ability has increased from 15,000 to 13,317,000 metric tons in 20 years. There will be around 5 million tonnes of demand per year, and there will be 11.3 million tonnes of capacity available worldwide, according to estimates. Asia has the most prominent ability for Dimethyl ether demand growth.

Research and analysis in this field have shown a steady increase in recent years. The majority of DMEs currently on the market are produced in developed countries. There are also new contenders for capability development, such as Ethiopia, Russia, Libya, Iran and Tashkent. Year-on-year capacity and production climbed by 96% in China between 2002 and 2006 and 97% between 2002 and 2006. Furthermore, China has proposed a manufacturing capacity of 20 million tonnes of DME by 2020[18, 19], which would be the world's largest.

#### 2.3 DME-An Alternative FuelEntrant

DME has a high volume of octane and is characterized by fast vaporization during theinjection. It has a low fuel injection pressure of about 200 atm due to this characteristic. However, the required diesel injection pressure is more significant than 1,200 atm. One of the most critical criteria for comparing this to other conventional fuels is well-to-tank (WTT) efficiency. In **Fig. 4**, the WTT effectiveness of petroleum-based powers is almost 90% by consuming the highest values. But WTT of DME exceeds slightly 70% [23].

DME is the gasoline that is ecologically responsible, and that is its benefit over the other hydrocarbons. The Nitrogen and Carbon emissions from DME vehicles are smaller than those from electricity (GTL) and electric motors, respectively.. Diesel and gas liquefaction, CO emissions are lower at low loads, but diesel and GTL CO emissions show substantial increases in CO emissions (Fig. 2-3). Conversely, by increasing the load, the CO emissions of DME remain at the same amount. DME has the lowest emission with comparison to diesel and GTL at low loads. NOx emissions are increased by high load levels for all kind offuels, but even Dimethyl ether has low excretion Fig (2-4).



Figure 2-1 Elimination of CO by a diesel engine running on GTL and DME at 1400 rpm



Figure 2-2 Elimination of NO by a diesel engine running on GTL and DME at 1400 rpm

#### 2.4 Gas to Liquids Conversion for DME

In the GTL method, there are mainly three phases. The first step is to manufacture natural gas syngas (CO and H2 combination). The second phase of GTL involves using a Fisher-Tropsch catalyst to convert biogas into gaseous fuels in other processes. The last stage is the improvement of the output of the reactor by the employment of splitting and hydro higher membrane to finish products [27, 28]. Porous carbon resources such as fuels, coke, natural gas and biofuels could produce syngas in the GTL process. On the other hand, natural gas is the most widely used feedstock in the sector because of its economic advantages over other feedstock's [29].



Figure 2-3 A schematic GTL process.

The popular staples of the GTL process [31] are petrol engines, fuel oil, gasoline (LPG), core oil and shellac, and hydrocarbons such as propylene and gushing smashing. Items removed have favourable properties such as low levels of sulphur and organic acids and low levels of toxic gases, carbon monoxide, compounds, and other particles emissions. These criteria allow this to be regarded as an environmentally friendly operation, and because of these benefits, GTL has recently received a lot of attention[32]. Fig. Fig. 3-2 illustrates the possibilities and difficulties of the extraction process.

#### 2.5 Syngas Reforming of GTL Process

The reshaping portion is the 1<sup>st</sup> move in the GTL procedure, as well as the primary method of syngas processing in the sector is the standarding of natural gas. In particular, there are 4 different types of reform: partly oxidizing, steaming reform, dryness reform, and mixtures of these modifications. The key reasons for picking reform styles or types are procedure goals, material availability, oil reserves, final result, nutritional requirements, security and ecological problems [34].

#### 2.5.1 Gasification Reactions

CO and H2 form the primary components of syngas. The Hydrogen to carbon monoxide ratio is measured by the heat of the system, the composition, and the reforming agent. The techniques used in the industry for repairing systems are steams repairing, partial oxidation, dryness reestablishing and reversible heat reforming.

#### 2.5.2 Partial Oxidation of CH<sub>4</sub>

The partial oxidation reaction is exo because heat is evolved and the duration of system is very short (Ital = 3.6-72 ms). Between methane and oxygen the overall response is;

$$CH + 0.5O = CO + 2H = H \circ 298K = -36 \text{ kJ/mol} (13)$$
-

Partly oxidizing gases formed a 2:1 ratio of Hydrogen and carbon monoxide : CO. The CH4 transformation elevating as the temperature increases (Fig 3-3)[34].



Figure 2-4 Effect of temperature on equilibrium for POX. (CH4:O2 = 1:0.5) P = 1 bar .



Figure 2-5 Effect of temperature on equilibrium for SR. (CH4: H2O = 1:1) P = 1 bar The response is endothermic, requiring less pressure and elevated thermal reading.

The reaction can be seen as follows:

CO 2 + CH 4 ?? 2CO + 2H 2 ~Hr = 247 kJ/mol (3-4)

The ratio of H2:CO is theoretically around 1:1 formed as a result of this reaction. When H2 and CO are heated to high temperatures, they are converted more quickly and completely.



Figure 2-6The impact of reaction on the equilibrium state of hydrogen production.

#### 2.5.3 CO2 Revolutionising via Autothermal Reformation

In order to achieve the required H2:CO ratio, this kind of reactor uses a mix of burning and vapor reforming.

The responses to auto thermal reforming are;

CH<sub>4</sub> + 1.5CO 2H<sub>2</sub>O 298K = -519 kJ/mol(53)CH<sub>4</sub> + H<sub>2</sub>COx + 3H<sub>2</sub>xH<sub>2</sub>O+ CO 298K = 206 kJ/mol (3-6) CO + H<sub>2</sub>O CO<sub>2</sub> + H<sub>2</sub>? 298K = -41 kJ/mol(73)

Through the combined use ofAuto thermo reformer, solvothermal, and ethylene oxide are all examples of chemical processes enables enhanced

Regulation of temperature inside the reactor. It also offers the opportunity to provide the ratio required Around H<sub>2</sub>: CO.

#### 2.6 GTL Process Catalysts

The most important types of catalysts used in reforming processes are supporting metal, chromium, and ferrous catalysis, supporting metal oxide hydrocarbons, and metaloxides carbide catalytic, to name a few examples. Deactivation of the catalyst happens during syngas processing as a result of carbon deposition. Consequently, numerous investigations of aid modifications are conducted to enhance the accuracy of the catalytic. Ni/Al<sub>2</sub>O is the most popular catalysts employed in the team development thanks to its low prices and easy sales frequency[35].



Figure 2-7 Fischer-Tropsch reactors .

#### 2.7 Product Upgrading

Goods such as GTL produced via FT processes are upgraded to much more appropriate interventions in the item upgrade segment. While carrying out the FT reactions, significant amounts of heavy waxes are created, and these heavy waxes are eventually converted into more usable hydrocarbons by the hydro-cracking process [33].

Hydrocracking is a method for breaking C-C bonds in heavy hydrocarbons, resulting in smaller molecules' formation. For GTL commodities, it is easier to perform the dehydrogenation process because the products are devoid of Sulphur, N-14 and aromatic substances[36].

#### Table 2-2 GTL products and services

GTL products	Services	
Naphtha	Petrochemical	
Diesel	Transportation	
Jet fuel	Air transportation	
Wax/lube	Lubricant	

#### Table 3 GTL products and services.

#### 2.8 DME Market

New developments in DME technology and the construction of new plants have been increasing worldwide[30]. Oil Company, British Petroleum, Chevron, BP, Syntroleum, Rentech, and Conoco are big businesses capable of operating sizable GTL plants [39]. As can be shown, the total capacity of DME plants increased enormously between 2006 and 2011. The rise will also begin to crescendo[31].

Recent studies have shown that the global demand for transport fuel for DME will rise. For example, during 2012 and 2035, gasoline consumption is predicted to rise between 26 million tons per day to 38 million tonnes each day, a 12% increase. (Figure 3-11). Transport fuels are the core industry for GTL. Therefore, GTL technology has a promising career to keep up with the increasing requirement [33, 37].



### Global product demand, 2010 and 2035

• Includes refinery fuel oil.

\*\* Includes bitumen, lubricants, waxes, still gas, sulphur, direct use of crude oil, etc.

Figure 2-8 Global product demand between 2010 and 2035

## Chapter 03 3 Process Modeling and Simulation 3.1 Direct DME Production

Pretreatment, modifying, fuels furnishes -reuses, Dimethyl ether blend, and detachment and decontamination of DME segments are part of the direct DME creation measure.



Figure 3-1 Block flow diagram Pretreatment Section

The cleansing of shale gas is the initial process in the formation of DME from it. The sample gas is first transported off a corrosive gas evacuation unit, as shown in Fig.4-2; dried-out measures are taken after that. The nitrogen expulsion unit, which is a layer detachment measure, is the next step. Two streams are formed in this cycle (Fig.4-3), an N-stream for resources and N-declined water for later creation steps. To recover flammable gas fluids, the nitrogen-depleted materials are sent off de-mechanized and then de-euthanized.



Figure 3-2 Flow diagram for gas production in general



Figure 3-3 The method of removing nitrogen

#### 3.1.1 Reforming Section

The following "section is referred to as transforming. As part of the product gas, gas is converted to biogas in this unit's reactor (a combination of CO and H2). The maximum temperature for incineration is about 800 degrees Celsius to 1800 degrees Celsius. Regardless, the degree of interaction is determined by the kind of feed and gasifier used [41, 42]. The data in Section 3.2.1 is organised into "several types of moment in time data."

For the direct production technique, dry improving methane was chosen as a changing form. For the immediate manufacturing procedure, dry improvement of methane was used as an altering type. The ratio of Hydrogen: CO is around 0.7 and 1 to efficiently manufacture DME from liquid fuels. Dry shifting plays an essential part in reformist response in this respect. Due to natural problems, dry transformation is enough to be acknowledged. By adjusting to methane owing to dry changes, Carbon can be transformed into considerable syngas. In either instance, since methane and CO2 are both stable particles, the dry changing of methane is thermodynamically negative. The organization of syngas needs a high response temperature. There have been various examinations recently that have demonstrated an increase in the appropriateness of dry improving. Consequently, some dry processing technologies, such as plasma procedures and chemical procedures, are available [42]. In both ordered collections of impulses used for dry methane improvement, reputable metal (Platinum, Palladium ) and nonhonourable progress metals are commonly maintained (Nickel, Cobalt, Iron). [43].

#### 3.1.2 **DME Synthesis Section**

240-280 °C and 30-70 bar are the response conditions in a direct union DME reactor. Table 4-1 list the general reactor conditions. The general consensus is that low temperatures and a high pressing factor help the harmony of reaction, which is exothermic. In aspects of generating DME from syngas, three steps take place at the same Time in the reactors:

> Methanol preparation  $CO + 2H_2 \rightarrow CH_3OH$   $\Delta H= -91 \text{ kJ/mol}$ Methanol dehydration:  $2CH3OH \rightarrow CH_3OCH_3 + H_2O$   $\Delta H=-23 \text{ kJ/mol}$ Water-gas shift reaction:  $CO + H_2O \rightarrow CO2 + H_2\Delta H= -41 \text{ kJ/mol}.$  (4-3) Overall reaction:  $3CO + 3H_2 \rightarrow CH_3OCH_3 + CO_2$   $\Delta H=-246 \text{ kJ/mol}$  (40)

methanol "preparation response most important response.CH3OH is formed when CO and H2 react. The methanol dries out as a result, and 2 moles of CH3OH react by delivering one-mole dimethyl ether and one-mole water. The water-gas change response, which generates carbon dioxide and hydrogen, is the third response. Three moles carbon monoxide and three moles hydrogen react to form one mole dimethyl ether and one mole carbon monoxide in" general.

Direct Dimethyl ether synthesis is possible in a variety of coating materials, including upflow, sludge, and repaired reactor. When Air Products and Sciences suggested the slurry step engine for invent new in 1991, the industry listened. The repaired nuclear and the deionization nuclear were touted as ideal reactors for use in nuclear power plants. Deionization reactor have a smaller propane magnetic fluids resistance than sludge neutrons and corrected nuclear plants, which makes sense because they are more compact.. DME's answer is highly exothermic. As a result, in a reactor, the elimination" of warmth and temperature control is essential. The effective binding of impetus constituents allows for fantastic temperature regulation in a fluidized-bed reactor [44].

#### 3.2 Separation, Purification and Recycle Sections

The basic idea behind that portion is the implementation of a reformer to separate CO2 and then send the CO2 back through the reformer to be reused. The architecture for CO2 reuse has three regions. The first comes from the corrosive gas evacuation device, the second from the transforming measure, and the third from the reuse of CO2 generated in the DME reactor. These three streams are consolidated and sent to a reformer, which produces CH4 for syngas production.

CO2 detachment innovations include retention, adsorption, cryogenic, and layer systems. The measure of Carbon dioxide in the actual structure, pattern of product that is pressing factor and heat, item virtue, item's final goal are all factors that influence creativity. Technologies have positive points and negative points. Reusability of sorbent and independence from the administrator are two advantages of retention. However, oxygen allows carbon steel offices to

consume oxygen, and NOx and SOx cause the dissolvable to become contaminated. Adsorption has the advantages of reusing the sorbent and having high working adaptability. Adsorption innovation cannot compensate for high CO2 convergence, but it can absorb more modest gases. Another breakthrough is cryogenic, which eliminates absorbent materials and relies on the barometrical critical element. However, to remove water, a few stages are needed, which increases the cost of interaction [46, 47].

On the traditional division steps, film structures are a promising competitor. This is especially advantageous for streams with far greater than 15percent Carbon dioxide and metal mills. There are no mechanical devices, and the emission must be regulated to function correctly.

Films and frameworks can instantly respond to several situations[46, 47].

Another issue to deal with is the extraction of undissolved syngas from reactors' output. The unburned syngas channel is separated into two surges, one used as fuel and the other re processes return at the Dimethyl ether system. After the combination of Dimethyl ether , alcohol, and freshwater is transported off the first stage of DME refinement, it is necessary to evaporate the mixture. In the second part of methanol refinement, vanished methanol is transported through a DME reactor to serve as a reaction product. The immediate blend course is depicted in Figure 16.



Figure 3-4 Directlyproduction cycle

#### 3.3 Manufacturing of Indirectly DME

Using an atypical approach, DME can be generated from shale gas in seven different ways (CH3OH -to-Dimethly ether ). These methods are systemic, improvement, gas washing, CH3OH mixture, identification, Dimethly ether union, and identification 2 (Fig.17).



Figure 3-5 Block flow diagram Pretreatment Portion

The repeated procedures as in directly manufacturing are carried out in this segment.

#### 3.3.1 Reforming Section

The incomplete "methane was oxidized and it was uses as a changing form in the roundabout technique's transforming section. The necessaryHydrogen to carbon monoxide ratio for backhanded strategy 2:1. With an H2/CO ratio of around 2 to 1.7, syngas can be generated. The water-gas change response is expected to arrive at the 2:1 proportion of syngas after incomplete"

oxidation transforming in this way.

The oxidation takes "place at temperatures ranging from 1300 to 1500°C and pressures of up to 70 bar. The carbon efficiency of the cycle is greater than 95%, and the contact methane slip is less than 1%.

1% of the population the syngas generated is almost entirely made up of H2, and CO. H2O, CO2, N2, and hints of hydrocarbons and nitrogen compounds make up the remaining 5%. Total oxidation can be both synergistic" and non-reactive [48].

#### 3.3.2 CH3OHP reparation

CH30H is "most probably the most important natural synthetic, due to the fact that it can deliver a wide range of synthetics. Synergist response is responsible for the majority of methanol delivery from syngas. Low temperatures and a strong pressing factor help the methanol response's harmony. Temperatures of 200-280 degrees Celsius and pressures of 50-99 atmospheres are ideal for a methane reactors (Table 4-2). During the synthesis of methanol, 2 sorts of processes take place in the furnace. The first reaction includes the reactions of freshwater and co gas, while the other process occurs the reactions of H and CO2 dioxide. Because of these two, one molar of alcohol is generated for every one molar of carbon monoxide, and two atoms of hydrogen are produced for every one molar of hydrogen. Table 3-1 Syngas to the CH3OH process condition

#### Table 4. Syngas to the CH30H process condition

Syngas to methanol	Conditions		
Temp (T) (°C)	200-280		
P(atm)	50-100		
H2: CO ratio	2		
Catalysts	CuO ZnO/A1 Do3		
Reaction types	Single or Multi-fixed bed adiabatic reactor Tubular, isothermal reactors		

The processes are happening in reactor;

 $CO(g) + H_2O(g) \rightarrow H_2(g) + CO_2(g)$ .  $\Delta H = -41 \text{ kJ/mol}$ 

 $CO_2\{(g)+3H2 \rightarrow CH; OH (l) +HO(g). \Delta H= -50 \text{ kJ/mol}$ 

**Overall reaction:** 

CO (g) +  $2H_2(g) \rightarrow CH_3OH \Delta H= -91 \text{ kJ/mol}$ 

Since "it may be polluted by tiny amounts of sulphur or halogens, the catalysis is the most important component of the ethanol production process. As a consequence, keeping excellent photocatalytic activity and selective requires a great amount of scrutiny to the enzyme. Methanol is an exothermic reaction, therefore heat should really be removed to enhance" conversion [49].


Figure 3-6 Process flow diagram

#### 3.3.3 Methanol dehydration:

 $2CH_3OH \leftrightarrow CH_3-O-CH_3 + H_2O \Delta H = -23.4 \text{ kJ/mol}$ 

#### 3.3.4 Separation, Purification and Recycle Sections

Carbon dioxide is removed from liquid fuels, and Carbon dioxide biogas is sent off the formaldehyde furnace to generate methanol from liquid fuels after the gasification generation stage.

After the methanol reactor has been passed, the unattained biogas is segregated and subdivided into two streams: recycling and fuel. Raw methanol is subsequently sent through the DME furnace. The combination of DME and separation2 is used in the separation2 region.

DME is isolated from the mixture in the DME processing segment, and methanol is then distillated in the methanol segment. Once more, distilled methanol is sent to the DME reactor. Figure 4-7 depicts a circuitous combination course.



Figure 3-7 Indirect synthesis route

Sub stream: MIXED	Mole Flow kmol/hr
CH3OH	5.356106
DIMETHYL	126.987
H2O	0.00497876
Mass Flow kg/hr	
CH3OH	171.6212
DIMETHYL	5850.167
H2O	0.0896937
Total Flow kmol/hr	132.348
Total Flow kg/hr	6021.878
Total Flow 1/hr	9759.02
Temperature C	50.20188
Pressure atm	11
Vapor Frac	0
Liquid Frac	1
Solid Frac	0
Enthalpy cal/mol	-47913.33
Enthalpy cal/gm	-1053.033
Enthalpy kcal/hr	-6341200
Entropy cal/mol-K	-72.02483
Entropy cal/gm-K	-1.582952
Density mol/cc	0.0135616
Density gm/cc	0.6170577
Average MW	45.50032

Table 3-2 Result of Simulation

# Chapter 04

# **4** Pinch Analysis of DME Process

## 4.1 Pinch Analysis Technique

- There are appreciated placement principle how we study cold and hot utilities and separation system and other process systems that are related to GCC and the pinch analysis.
- There is multiple level of hot and cold value level. The mixing of cooling and heating systems the optimally with this process.
- The Network optimization and relaxation there are modified a network to reduce and eliminate a small heat exchanger which are less cost effective.
- The retrofit of presence chemical plants that are adapting a technique to dealing an existing plant layout and exchanger.
- There is systems analysis of power and heat systems and refrigeration and heat pumps systems.
- There are causes of process change where changing operating conditions of different unit operations and other than stream to maximize the heat integration.

#### 4.1.1 Key Steps of Pinch Technology

There is four steps for pinch analysis in the design of heat regaining for both existing and new heat exchanger design.

• First, Data extraction that are involved in collection of data for the utility and process.

- Targeting the temperature which is best for the show in various respects.
- The design of heat exchanger where an initial warmth exchanger network is established.
- Last is optimization wherever the initial design is basic and enhanced economically.

### 4.1.2 Data Extraction



Figure 4-1 Steps Of Pinch Analyasis

## 4.2 Basic Element of Pinch Technology

- Hot Streams that required cooling medium. It is move in the right direction.
- Cold Streams that are required a heating medium. It is moving toward the left direction.
- A heat exchanger is represented by vertical lining joining the two open circles on the different streams being matched.

- Cooler and Heater are represented in an open process on the streamline being cooled and heated.
- The temperatures that can be put on the grid are easily checked on terminal difference temperature for each one unit.



Figure 4.2 grid of Pinch Analysis



Figure 4.3 Composite Curve

## 4.3 Pinch Technologyvs Process Engineering

- Pinch Technology is a subdivision of process engineering.
- Our engineer are specialized information of thermodynamic and software tools. They can communicate effectively with clients and conceptual design.
- Carrying out process engineering project without the input of pinch study will led a less efficient.

### 4.3.1 How a pinch technology is different from other energy

A pinch technology is used to saving and their corresponding financial benefits.

• Maximum possibility to saving utilities.

- It study at all generally site
- It reveals the highest cogeneration potential.
- It does not include bench-mark but also account all specific factors, age, process equipment, cost product ECT.

## 4.3.2 Roleof Thermodynamic Lawin Pinch Technology

- Real Saving
- Feasible job
- significant Target

## 4.3.3 Important of Pinch Technology

- Pinch give best that will be achieved in systems.
- Pinch can gives the target to aim for that is less than theoretical maximum.
- The target is set the basic of heat exchanger design and also gives rules about how to design.
- Take place at wide systems. This allows seeing the interaction of two streams in process flow diagram or the utility flow sheet.
- Refine the area data where the accuracy factor is important. Pinch can show incomplete data.
- Pinch Analysis can compared results with other design tools, which can require detailed knowledge about geometry and flowsheet structure.
- Pinch is one of the best tools that can be used for conceptual design.

Problem Addressed by Pinch Technology

## 4.3.4 Application of Process Intensification

- Heat Integration
- Cogeneration site targeting
- Fractional Distillation Column target
- Hydrogen gas management refinery



Figure 4-4 Potential Energy Saving

## 4.4 Methodology of Pinch Analysis

Stream	Description	Туре	Heat Type	T1 (K)	T2 (K)	H (kW)	$m \cdot cp(kW \cdot K)$
1	Cold	Cold	Sensible	468.15	587.15	31825.	267.437
2	Hot	Hot	Sensible	1623.65	468.15	-39209.7	33.9331
3	Hot	Hot	Sensible	587.15	448.15	-49001.4	352.528
4	Cold	Cold	Sensible	448.5	507.5	33477.1	567.408

Table 0-1 Stream	n Table of	DME Process:
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On the basis of a sufficient heat exchange, the thermometer intervals graph was drawn. The utilities

aim has been identified, and streaming splitter technologies has been used to set up a connection to reach it.



## 4.5 Grid Diagram



Table 4-2 Temperature	Interval Diagram
-----------------------	------------------

Temperature (K)	Enthalpy (kW)
1618.65	0.
592.15	34832.3
582.15	32497.3
512.5	40787.3
502.15	36146.6
473.15	36304.2
463.15	39032.9
453.5	41338.7
443.15	49684.4
428.15	56491.7



## Cascade calculated with the Problem Table Algorithm

Figure 4-5 Heat Exchanger Network



Figure 4.6 Heat Exchanger Network

Table 4-3 Analysis of Heat Exchanger Network

	Lowest	Available	Left behind	Totals
Amount of H.E.	5	5	0	5
Area (m <sup>2</sup> )	606.371	736.098	0.	736.098
Capital Cost (\$/año)	663924	644000	19671.8	663671
Heating (kW)	0.	0.	0.	0.
Cooling (kW)	56491.7	56491.4	0.	56491.4

# **Chapter 05**

# 5 Cost Analysis

## 5.1 Cost Analysis of DME Process

A capital cost is cost that associate with existing chemical plant and modification of new chemical plant.

#### 5.1.1 Order of Magnitude

These cost information is adjust by using scaling factor, capacity, and for providing the estimate cost of chemical plant. A systemic flowing pattern is used for the order of Magnitude cost estimation.

#### 5.1.2 Study Estimation

In this type of cost estimation, enlist a major components found in the process industry. These are including equipment like compressor, pump-turbine, heat exchanger ECT. The each. The kit is. Roughly sized. and determined the cost estimation. This estimation is based on a process flow diagram.

#### 5.1.3 Preliminary Design Estimate

In these sort estimation, the exact sizing of equipment that is used in study estimate is essential. The introduction also estimates pattern of instruments is made up of pipes, electrical appliances, and instruments and utilities. The initial figure is based on a process flow diagram which comprised equipment stretches, height diagram.

#### 5.1.4 Definitive Estimation

This estimation requires preliminary specification of all chemical equipment,

instrumentation, utilities and off-site. The definitive estimate is including the Process FlowDiagram, utility balance, and P&ID.

## **5.2 Detailed Estimation**

In this types of estimate that require total.mechanics of the.method .and also coordinated all the .utilities like an off-site instrument. In detailed estimation, it includes Process Flow. Diagram,Process and.Instrumentation.Diagram, utility balance.and vessel sketches.

Class of Estimate	Level of Project Definition (as % of Complete Definition)	Typical Purpose of Estimate	Methodology (Estimating Method)	Expected Accuracy Range (+/- Range Relative to Best Index of 1)	Preparation Effort (Relative to Lowest Cost Index of 1)
Class 5	0% to 2%	Screening or Feasibility	Stochastic or Judgment	4 to 20	1
Class 4	1% to 15%	Concept Study or Feasibility	Primarily Stochastic	3 to 12	2 to 4
Class 3	10% to 40%	Budget, Authorization, or Control	Mixed but Primarily Stochastic	2 to 6	3 to 10
Class 2	30% to 70%	Control or Bid/Tender	Primarily Deterministic	1 to 3	5 to 20
Class 1	50% to 100%	Check Estimate or Bid/Tender	Deterministic	1	10 to 100

Figure	5-0-	-11	List	of	Cost	Estim	ation
--------	------	-----	------	----	------	-------	-------

The level of accuracy of the estimate is depending upon:

- Effort and Time available
- Technique and Method Employed
- What is the Qualification of the estimator
- Study sensitivity of different parameter

## 5.3 Costing Technique of Module

The preliminary cost estimation is best for chemical plant. This technique is based on all costs back of purchased cost of chemical equipment evaluation. There is some technique of Module costing:

- Specify equipment types.
- There is specific equipment pressure.
- There is specific material of construction.



Figure 5-0-2 Accuracy of Cost Revenue Estimator Vs Cost of Making

## 5.4 Source of Cost Estimation

The information of cost analysis is helpful for cost and revenue estimating. There are four main Source of information.

- Accounting Record
- Other sources take from firm
- Source from outside the firm
- Research and Development

## 5.5 Accounting Record

An accounting record is the primary source.of.information.for cost analysis but they.are.notsuitable.for.direct.use. An accounting record is consisting of series of operating procedures for saving and keeping record of complex transactions between establishes categories of different assets. Accounting record is the Source.of.historical.data. But there is some limitation when they are used. In the making. Prospective estimation for economic. Engineering analysis.

#### 5.5.1 Other Source takes from the firm

There are several people and records that are the best Source for estimating information. For Example, Firms that keep the previous record useful to economic analysis are engineering, quality, purchased, sales, and personnel.

#### 5.5.2 Source takes form outside firm.

Different Sources are outside the firm that is helpful information for cost analysis. The primary sources from an outsider are:

- Published Information
- Current Wage

## 5.6 Research and Development

This information. Is.not given or published. And. It cannot be. They were obtained by. it was

consulting and the. only alternative. May be. Undertake Research and Development to generate data. First developed a pilot plant and observing the operating condition and pressure.



Figure 5-0-3 The cash flow diagram for industrial operation

## 5.7 Factor Affecting Investmentand Production Cost

Whenever an Engineer of a Chemical is decided the cost of any product, this cost must be accurate to a reliable decision. The engineer must know the factor that affects the price of the

product. Many companies have a different arrangement with another contractor, whereas raw material and equipment may be purchased lower than market value, but a chemical engineer is based on the raw material of reactant that is available in the market place. The engineer must to be upgraded with price fluctuation, governmental regulation, company policies and another factor.

• Source of Equipment

#### 5.7.1 Price Fluctuation

In the modern technology, there are price fluctuation price is varies from period to period. The labour cost is changed by changing the price of food and goods. Therefore a chemical engineer should know the daily price and wage fluctuation.

## 5.7.2 Company Policy

The policy of the company is a direct effect on the cost of the product. The company policies depend on labour unions because there is an effect of labour charge overtime work and the operator and engineer that work in a company in overtime work.

#### 5.7.3 Governmental Policy

The government has many regulations and rules that are cause-effect on the direct cost of industrial processes. For example, there is some tariff regulation on imports and export. There are restrictions on permissible depreciation rates and environmental law.



Figure 5-0-4 Breakeven point for chemical plant

#### **Grass Root Plant**

A grass root plant is consisting of complete plant installed on new side. This investment included all cost of land.

#### **Battery Limit Plant**

A boundary limits plant that define plant limit where it start from the production. A battery limit plant is the point where plant inlet is start from there. It include all the process equipment but exclusion of storage, Administration building, Auxiliary facilities.



Figure 5-0-5 Application of six-tenth-factor rule to the cost

## 5.8 General Overall Design of Chemical Plant

- We study the plant location.
- We study instrumentation control and chemical process.
- We study external utilities that used in chemical process.
- We study the different 3D diagram of chemical process.
- We study the structural design and building of chemical process.
- We study the handling of different material through different process

	Exchanger Type	Shell Pressure (barg)	Tube Pressure (barg)		Area (square meters)	Bare Module Cost
E-101	Floating Head	2	2		99.4	\$ 128,000
E-102	Floating Head	2	2		106	\$ 132,000
E-103	Floating Head	2	2		171	\$ 168,000
E-104	Floating Head	2	2		83	\$ 120,000
E-105	Floating Head	11	11		102	\$ 131,00
E-106	Fixed, Sheet, or U-Tube	11	11		22.7	\$ 84,300
E-107	Floating Head	2	2		22	\$ 93,100
E-108	Floating Head	1	2		22.8	\$ 93,100
Pumps (with drives)	Pump Type	Power (kilowatts)	# Spares	мос		Bare Modul Cost
P-101	Centrifugal	7.2	0	Carbon Steel		\$ 21,700
P-102	Centrifugal	5.2	0	Carbon Steel		\$ 19,800
P-103	Centrifugal	1	0	Carbon Steel		\$

## 5.9 Equipment Summary of DME Process

Figure 5-6 Equipment Summary of DME Process

## 5.10 Utilities Summary of DME Process

÷					
Name	Total Module Cost	Grass Roots Cost	Utility Used	Actual Usage	Annual Utility Cost
	0031	0031			0051
E-101	\$ 151,565	\$ 216,000	Medium- Pressure Steam	14400 MJ/h	\$ 1,700,000
E-102	\$ 156,000	\$ 222,000	Low- Pressure Steam	2030 MJ/h	\$ 224,300
E-103	\$ 199,000	\$ 283,000	Medium- Pressure Steam	12400 MJ/h	\$ 1,467,000
E-104	\$ 141,000	\$ 201,000	Medium- Pressure Steam	2490 MJ/h	\$ 294,000
E-105	\$ 155,000	\$ 220,000	Medium- Pressure Steam	3140 MJ/h	\$ 370,800
E-106	\$ 99,000	\$ 141,000	Medium- Pressure Steam	5790 MJ/h	\$ 683,700
E-107	\$ 110,000	\$ 156,000	Medium- Pressure Steam	5670 MJ/h	\$ 669,600
E-108	\$ 110,000	\$ 156,000	Medium- Pressure Steam	1200 MJ/h	\$ 141,710
P-101	\$ 25 700	\$ 34 500	Electricity	10.3 kilowatts	\$ 5 180

Figure 5-0-7 Utilities Summary Of DME Process Material of Construction

Material Name	Classification	Price	Flowrate (kg/h)	Annual Cost
		(\$/kg)		
DME	Product	\$	130000.00	\$
		(0.05)		(54,093,000)
METHANOL	Raw Material	\$	8370.00	\$
		0.01		975,172
WATER	Raw Material	\$	2500.00	\$
		0.00		20,805

Figure 5-0-8 Material of Construction

## 5.11 Cash Flow Diagram



Figure 5-0-9 Cash Flow Diagram

## 5.12 Discount andNon-Discount Profitability Criteria

Discounted Profitibility Criterion	-	Non-Discounted Profitil	oility Criteri
Net Present Value (millions) 143.08		Cumulative Cash Position (millions)	427.67
Discounted Cash Flow Rate of Return 24.62%		Rate of Return on Investment	28.51%
Discounted Payback Period (years) 2.9		Payback Period (years)	2.2

Year Investme			d		ECL ed	D		COM	/D COM_d \*/1 +\ud	Cash Flow	Cash Flow	Cumulative Cash Flow	Cumulative Cash Flow
rear	investmen	L	uk		ruil-suk	ĸ		COM	(R-COMd-uk) (1-1)+0	<sup>k</sup> (Non-discounted)	(discounted)	(discounted)	(Non-discounted)
	0 1	0.00			150.00					(10.00)	(10.00)	(10.00)	(10.00)
	1 9	0.00			150.00					(90.00)	(81.82)	(91.82)	(100.00)
	2 9	8.10			150.00					(98.10)	(81.07)	(172.89)	(198.10)
	3			30.00	120.00	4	06.01	314.75	63.69	63.69	47.85	(125.04)	(134.41)
	4			48.00	72.00	4	06.01	314.75	71.79	71.79	49.03	(76.00)	(62.62)
	5			28.80	43.20	4	06.01	314.75	63.15	63.15	39.21	(36.79)	0.54
	6			17.25	25.95	4	06.01	314.75	57.95	57.95	32.71	(4.08)	58.49
	7			17.25	8.70	4	06.01	314.75	57.95	57.95	29.74	25.66	116.45
1	8			8.70	-	4	06.01	314.75	54.11	54.11	25.24	50.90	170.55
	9				-	4	06.01	314.75	50.19	50.19	21.29	72.19	220.74
1	0				-	4	06.01	314.75	50.19	50.19	19.35	91.54	270.94
1	1				-	4	06.01	314.75	50.19	50.19	17.59	109.13	321.13
1	2				-	4	06.01	314.75	58.44	106.54	33.95	143.08	427.67

Figure 5-0-10 Discount and Non-Discount Profitabity Criteria

# 5.13 Variable Key Parameter over Plant Life

	Lower Limit	Upper Limit	<u>Base Value</u>
FCIL	-20%	30%	\$ 150,000,000
Price of Product	-20%	5%	\$ 406,011,239
Working Capital	0%	0%	\$ 38,100,000
Income Tax Rate*	0%	0%	45%
Interest Rate*	0%	0%	10%
Raw Material Price	-10%	10%	\$ 229,953,504
Salvage Value	0%	0%	\$ 15,000,000

Figure 5-0-11 Variable Parameter Over Plant Life

# Chapter 06

## 6 Analysis of Cost Improvement 6.1 Cost Improvement

In the R&D and design of chemical plant the capital cost are universal estimation. In the chemical plant performance is overestimated. The product cost is trending to increasing significant between realized cost and estimate. There are number of factor that depends upon decrease cost of chemical plant.

- Improving the Technology
- Learning by designer and plant operator
- Economic analysis of large equipment
- Using the cheap raw material cost

This is relationship between better worker performance and decreased cost and improved management and production and technical improvement. This phenomenon is types of manufacturing process are called learning curve. The learning phenomena are not factor that promote the relationship between declined cost unit and cumulative production. There are generic factor of learning improvement are learning by plant improvement, improvement the technical ability, improved the economic scale and decrease raw material cost.

## 6.2 Rateof Cost Improvement

The rate of Cost Improvement is defined as there are same manner of as the learning curve. There are slope of regression between fitted logarithm cost on Y-axis and logarithm of industry production on X-axis.

$$Cn = C1$$

The curve of improvement is 100% is minus with rate of improvement. If the rate of improvement is 20% then rate of curve is 80%.

#### 6.2.1 Factor AffectRateof Improvement

- The characterize the Technology
- The characterize the marketplace
- The characterize the management

The first factor is important for rate of improvement because of the state of product and market product and other factor cause less variant in product technology.

We are considering 4 hypotheses that are regarding relationship between cost improvement and technical characterizes.

**The higher level of complexity are cause high improvement** The hypothesis are implies that higher the number of complexity cause the higher number of interlink step process and it offer greater the number of opportunities to improve the process. The more step are implied to improvement through process simplification and it causes higher proficiency.

• If product has price it causes less cost improvement

Higher the capital investment is causes rapid improvement in chemical process because process will provide less value of performance and it also cause less cost improvement.

#### Solid processing is may related to rapid cost improvement

Solid process is involved more physical unit operation other than gas and liquid and physical operation involve in less technological improvement. The solid processes are weak as compared to gas processing. There are some elementary factor in which heat and material balance are more difficult to take extrapolate from one plant to next changes. There is less show of improvement in solid processing.

#### In Technological display greater economical scale show more rapid improvement in cost

There is relationship between learning curve and technological innovation and other economical scale are discussed in context of CPI. A learning improvement are implies in the state of art of product, labor, improved management and organization and an advance product technology. Economic scale is shown range of cost unit decline as well as level of production increments.



Figure 6-1 Scale Economic with and without technical change

### 6.3 Factor that Affect Characterize the Market Place

There are three hypotheses that are relationship between market factor and cost improvement.

#### • The actual change feedstock prices will effect of improvement cost

The hypothesis is show that cost improvement in raw material will be reelected the more rapid in production improvement. The cost improvement is most rapid for intermediate rather than primary chemical used. The predecessor chemical are causes more rapid cost improvement.

- The higher demand of growth are causes more rapid learning because of higher demand will create powerful incentive to power reduced cost to capture market value.
- The concentration Level and competition in industry may affect cost improvement.

Some of the economic told that concentration has reduced the incentive investment in the Research and Development Department.

### 6.3.1 Factor that are characterize the Management

The management has cause more affect in cost improvement but they are cause effect in management. This relation is hard to prove. However there are two hypotheses.

- The higher level of R&D is causes more rapid cost improvement.
- We can do careful management to maximizing collect information from earlier chemical plant and provided continuity for follow up plant and that effect rate of cost improvement after commercialization of new process or market product.

#### 6.4 Understanding Cost Improvement in Chemical Processing

There are 37 chemical process and products that are factor associated with cost improvement. First examine hypotheses that related to Technology, Marketplace, management and analysis cost improvement that is form of database. Whenever data is not found then we can used case studies and literature value to discuss factors qualitatively and finally present statistical model for cost improvement in chemical process industry and also analyze a chemical model to test hypotheses. The cost improvement slope is based on chemical processes in database.

#### 6.4.1 Chemical Type

The purpose of this analysis is binary in chemical types. There are correlation of this confirm result. The rate of the improvement for metal component is very poor. In the practical rate of other chemical types which are very similar to each other.

#### 6.4.2 Capital Intensity

The capital makes big contribution on product cost have caused more rapid economic improvement is not sure by the cost analysis. There are two relationships way between cost improvement and cost analysis that could support the factors that actually cause cost improvement , better management , technological innovation ect that can have limit effect on the feedstock costs but they have potentially have great effect on the capital cost.

#### 6.4.3 Process Factor

There are no relationship between "scaling factor" and cost improvement for technological analysis. The scaling factor is measure economics scale analysis of capital cost. The most important factor is cost of chemical. There is relationship between cost improvement slope and cost economies after other factor are controlled variable

Chemical Type	Average Capital Cost per Pound, as a Percent of 1969 Product Price
Organics	18.7
Inorganics	26.9
Fibers	29.3
Metals	28.0
All	21.3

Table 6-1 Capital Intensity of Different Chemical Groups

#### 6.4.4 Process Complexity

The process Complexity has offered more opportunity for improvement of technical processes by using complexity methods.

## 6.5 Cost Improvement and Marketplace

The price change in feedstock are causes big effect on prices cost on product. There is most implication that is applied on cost analysis.

- We are expecting that there is less cost improvement in primary chemicals as compare to secondary chemical. The refined chemical raw material will be less variable therefore that improving the reliability the chemical process. In the addition there are causes opportunity for introducing feedstock and that are greater than secondary chemical involved.
- There is prediction that the rate of cost improvement in primary chemical cost is faster than improvement in secondary chemicals.
- There are expecting that less cost improvement in feedstock where rising cost are associates with mineral depletion

Factor <sup>a</sup>	Pearson Correlation	Statistical Significance
Cost improvement slope of precursor chemical (19)	+0.60	0.006
Product is a "secondary" chemical (37)	-0.43	0.009
Process uses "raw" solid feedstock (41)	+0.55	0.0005

Table 6-2 Correlation between Improvement Slopes and Feed Stock Factor

\*Numbers of observations are shown in parentheses.

### 6.6 Cost Improvement and Management

In the first hypotheses there are relationship between cost improvement and industrial management for the chemical process. They are cause higher level of development and research expenditure of product cost and it causes rapid improvement. The second hypotheses are on management information transfer and organization of rapid improvement cost.

## 6.7 Cost Improvement and R&D Expenditure

There is magnitude of relationship between R&D expenditure and cost improvement has very important implication of industrial competitiveness. We have hoped to test relationship between different R&D expenditure on refinement of different processes and cost improvement slopes by using different multiple regression model.

• Lieberman Equation cannot contain four factors that are use to drove the cost improvement in the chemical processes. This relationship would affect the factors that are taken to unknowns.

- R&D is cause significant contribution to examine and explain cost improvement variation, which are combined cumulative industry output and strongly related with cost analysis. The relationship between cost improvement and the cumulative result is much stronger than R&D expenditure and also cost analysis.
- Lieberman has a measure of R&D expenditure that admittedly the crude. It is the ratio of sale of R&D expenditure and company sales. There is a causal linked between cost improvement and R&D expenditure.

Blender Data						
Blender Type	$\mathbf{K}_1$	$K_2$	<b>K</b> <sub>3</sub>	$V_{min}(m^3)$	$V_{max}(m^3)$	F <sub>BM</sub>
Kneader	5.0141	0.5867	0.3224	0.14	3	1.12
Ribbon	4.1366	0.5072	0.0070	0.70	11	1.12
Rotary	4.1366	0.5072	0.0070	0.70	11	1.12

Centrifuge Data						
Centrifuge Type	$\mathbf{K}_1$	$K_2$	<b>K</b> <sub>3</sub>	D <sub>min</sub> (m)	D <sub>max</sub> (m)	F <sub>BM</sub>
Auto Batch Seperator	4.7681	0.9740	0.0240	0.50	1.70	1.57
Centrifugal Seperator	4.3612	0.8764	-0.0049	0.50	1.00	1.57
Oscillating Screen	4.8600	0.3340	0.1063	0.50	1.10	1.57
Solid Bowl w/o Motor	4.9697	1.1689	0.0038	0.30	2.00	1.27

Compressor Data (without electric motors)							
Compressor Type	$\mathbf{K}_1$	$K_2$	$K_3$	F <sub>BMCS</sub>	F <sub>BMSS</sub>	F <sub>BMNi</sub>	W <sub>min</sub> (
Centrifugal	2.2891	1.3604	-0.1027	2.7	5.8	11.5	45
Axial	2.2891	1.3604	-0.1027	3.8	8.0	15.9	45
Rotary	5.0355	-1.8002	0.8253	2.4	5.0	9.9	18
Reciprocating	2.2891	1.3604	-0.1027	3.4	7.0	13.9	45

Conveyor Data						
Conveyor Type	$\mathbf{K}_1$	$K_2$	<b>K</b> <sub>3</sub>	$A_{min}(m^2)$	$A_{max}(m^2)$	FBM
Apron	3.9255	0.5039	0.1506	1.00	15.00	2
Belt	4.0637	0.2584	0.1550	0.50	325.00	1.25
Pneumatic	4.6616	0.3205	0.0638	0.75	65.00	1.25
Screw	3.6062	0.2659	0.1982	0.50	30.00	1.1

Crystallizer Data						
Crystallizer Type	$K_1$	$K_2$	<b>K</b> <sub>3</sub>	$V_{min}(m^3)$	$V_{max}(m^3)$	F <sub>BM</sub>
Batch	4.5097	0.1731	0.1344	1.50	30.00	1.6

**Drive Data** 

Electric Drives	<b>K</b> <sub>1</sub>	$K_2$	K <sub>3</sub>	$F_{BM}$	W <sub>min</sub> (kW)	W <sub>max</sub> (kW)
Explosion Proof	2.4604	1.4191	-0.1798	1.5	75	2600
Totally Enclosed	1.956	1.7142	-0.2282	1.5	75	2600
Open/Drip Proof	2.9508	1.0688	-0.1315	1.5	75	2600
Non-Electric Drives	$K_1$	$K_2$	<b>K</b> <sub>3</sub>	$F_{BM}$	W <sub>min</sub> (kW)	W <sub>max</sub> (kW)
	-					
Gas Turbine	21.7702	13.2175	-1.5279	3.5	7500	23000
Steam Turbine	2.6259	1.4398	-0.1776	3.5	70	7500
Internal Combustion	2.7635	0.8574	-0.0098	2.0	10	10000

Dryer Data						
Dryer Type	$K_1$	$K_2$	<b>K</b> <sub>3</sub>	$A_{min}(m^2)$	$A_{max}(m^2)$	$F_{BM}$
Drum	4.5472	0.2731	0.1340	0.50	50.00	1.6
Rotary, Gas Fired	3.5645	1.1118	-0.0777	5.00	100.00	1.25
Tray	3.6951	0.5442	-0.1248	1.80	20.00	1.25

Dust Collectors Data						
Collector Type	$\mathbf{K}_1$	$K_2$	<b>K</b> <sub>3</sub>	$V_{min}(m^3/s)$	$V_{max}(m^3/s)$	F <sub>BM</sub>
Baghouse	4.5007	0.4182	0.0813	0.08	350.00	2.86
Cyclone Scrubbers	3.6298	0.5009	0.0411	0.06	200.00	2.86
( Centrifugal, Gravity						
Spray, Impingement,						
and Wet Dynamic)						
Electrostatic Precipitator	3.6298	0.5009	0.0411	0.06	200.00	2.86
Venturi	3.6298	0.5009	0.0411	0.06	200.00	2.86

Fan Data (include electric motors)							
Fan Type	$\mathbf{K}_1$	$K_2$	<b>K</b> <sub>3</sub>	F <sub>BMCS</sub>	FBMfiberglass	F <sub>BMSS</sub>	F <sub>BMNi</sub>

Centrifugal Radial Fan	3.5391	-0.3533	0.4477	2.7	5.0	5.8	11.5
Centrifugal Backward curved fan	3.3471	-0.0734	0.3090	2.7	5.0	5.8	11.5
Axial Tube Fan	3.0414	-0.3375	0.4722	2.7	5.0	5.8	11.5
Axial Vane Fan	3.1761	-0.1373	0.3414	2.7	5.0	5.8	11.5

Filter Data						
Filter Type	$K_1$	$K_2$	<b>K</b> <sub>3</sub>	$A_{min}(m^2)$	$A_{max}(m^2)$	FBM
Bent	5.1055	0.4999	0.0001	0.90	115.00	1.65
Cartridge	3.2107	0.7597	0.0027	15.00	200.00	1.65
Disc and Drum	4.8123	0.2858	0.0420	0.90	300.00	1.65
Gravity	4.2756	0.3520	0.0714	0.50	80.00	1.65
Leaf	3.8187	0.6235	0.0176	0.60	235.00	1.65
Pan	4.8123	0.2858	0.0420	0.90	300.00	1.65
Plate and Frame	4.2756	0.3520	0.0714	0.50	80.00	1.80
Table	5.1055	0.4999	0.0001	0.90	115.00	1.65
Tube	5.1055	0.4999	0.0001	0.90	115.00	1.54

Fired Heater Data							
Paactive Heaters	K.	K	K.	$\mathbf{O}$ : ( <b>kW</b> )	$\mathbf{O}$ (kW)	P <sub>max</sub> (barg	C.
Reformer Furnace	3.068	$\frac{K_2}{0.6597}$	<u> </u>	$\frac{Q_{\min}(K, \mathbf{v})}{3000}$	$\frac{Q_{\text{max}}(\mathbf{K} \mathbf{v})}{100000}$	200	$\frac{C_1}{0.1405}$
Reformer i uniace	5.000	0.0377	0.0174	5000	100000	200	0.1405
Pyrolysis Furnace	2.3859	0.9721	-0.0206	3000	100000	200	0.1017
						P <sub>max</sub> (barg	
Non-reactive Heaters	$K_1$	$K_2$	<b>K</b> <sub>3</sub>	Q <sub>min</sub> (kW)	Q <sub>max</sub> (kW)	)	$C_1$
Process Heater	7.3488	-1.1666	0.2028	1000	100000	200	0.1347

						P <sub>max</sub> (barg	
Thermal Fluid Heaters	$\mathbf{K}_1$	$K_2$	<b>K</b> <sub>3</sub>	Q <sub>min</sub> (kW)	Q <sub>max</sub> (kW)	)	$C_1$
Hot Water	2.0829	0.9074	-0.0243	650	10750	200	-0.0163
Molten Salt, Mineral Oil,	1.1979	1.4782	-0.0958	650	10750	200	-0.0163
Diphenyl Based Oils	2.2628	0.8581	0.0003	650	10750	200	-0.0163
Packaged Steam Boilers	6.9617	-1.48	0.3161	1200	9400	40	2.5941
Evaporator Data							
Evaporator Types	K1	K <sub>2</sub>	K3	$A_{\min(m^2)}$	$A_{max(m2)}$	Pmax(harg)	$\mathbf{C}_1$
Forced Circulation	5.0238	0.3475	0.0703	5	1000	150	0.1578
Falling Film	3.9119	0.8627	-0.0088	50	500	150	0.1578
Agitated (Scraped Wall)	5	0.149	-0.0134	0.5	5	150	0.1578
Short Tube	5.2366	-0.6572	0.35	10	100	150	0.1578
Long Tube	4.642	0.3698	0.0025	100	10000	150	0.1578
Heat Exchanger Data							
Exchager Type	$\mathbf{K}_1$	$K_2$	<b>K</b> <sub>3</sub>	$C_1$	$C_2$	$C_3$	$B_1$
Double Pipe	3.3444	0.2745	-0.0472	13.1467	-12.6574	3.0705	1.74
40 barg< P < 100 barg				0.6072	-0.912	0.3327	
P < 40 barg				0	0	0	
Multiple Pipe	2.7652	0.7282	0.0783	13.1467	-12.6574	3.0705	1.74
40 barg< P < 100 barg				0.6072	-0.912	0.3327	
P < 40 barg				0	0	0	
Fixed tube, sheet, or U tube	4.3247	-0.303	0.1634	0.03881	-0.11272	0.08183	1.63
tubes only $> 5$ barg				-0.00164	-0.00627	0.0123	
Floating Head	4.8306	-0.8509	0.3187	0.03881	-0.11272	0.08183	1.63
tubes only > 5barg				-0.00164	-0.00627	0.0123	
Bayonet	4.2768	-0.0495	0.1431	0.03881	-0.11272	0.08183	1.63
tubes only $> 5$ barg Kettle Reboiler tubes only $> 5$ barg	4.4646	-0.5277	0.3955	-0.00164 0.03881 -0.00164	-0.00627 -0.11272 -0.00627	0.0123 0.08183 0.0123	1.63
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Scraped Wall	3.7803	0.8569	0.0349	13.1467	-12.6574	3.0705	1.74
40 barg< P < 100 barg				0.6072	-0.912	0.3327	
P < 40 barg				0	0	0	
Teflon Tube	3.8062	0.8924	-0.1671	0	0	0	1.63
Air Cooler	4.0336	0.2341	0.0497	-0.125	0.15361	-0.02861	0.96
Spiral Tube - shell and tube	3.9912	0.0668	0.243	-0.4045	0.1859	0	1.74
tube only				-0.2115	0.09717	0	
Spiral Plate	4.6561	-0.2947	0.2207	0	0	0	0.96
Flat Plate	4.6656	-0.1557	0.1547	0	0	0	0.96
Materail Factors, F <sub>M</sub>							
	Shell -						
	CS	CS	Cu	CS	SS	CS	Ni
	Tube -						
<u>Exchanger Type</u>	CS	Cu	Cu	SS	SS	Ni	Ni
Double Pipe	1.00	1.35	1.69	1.81	2.73	2.68	3.73
Multiple Pipe	1.00	1.35	1.69	1.81	2.73	2.68	3.73
Fixed tube, sheet, or U tube	1.00	1.35	1.69	1.81	2.73	2.68	3.73
Floating Head	1.00	1.35	1.69	1.81	2.73	2.68	3.73
Bayonet	1.00	1.35	1.69	1.81	2.73	2.68	3.73
Kettle Reboiler	1.00	1.35	1.69	1.81	2.73	2.68	3.73
Scraped Wall	1.00	1.35	1.69	1.81	2.73	2.68	3.73
Spiral Tube	1.00	1.35	1.69	1.81	2.73	2.68	3.73
	Shell N	Aaterail				7	
Exchanger Type	CS	Cu	SS	Ni	Ti		
Teflon Tube Exchanger	1.00	1.20	1.30	1.40	3.30		
	Mate	erial In Co	ntact with P	rocess Fluid			
Exchanger Type	CS	Cu	SS	Ni	Ti		
<u> </u>	00	~ ~	~~~		**	I	

Spiral Plate	1.00	1.35	2.45	2.68	4.63
Flat Plate	1.00	1.35	2.45	2.68	4.63
	Tube N	Iaterial			
Exchanger Type	CS	Al	SS		

Mixer Data						
<u>Mixer Type</u>	$\mathbf{K}_1$	$\mathbf{K}_2$	<b>K</b> <sub>3</sub>	P <sub>min</sub> (kW)	P <sub>max</sub> (kW)	FBM
Impeller	3.8511	0.7009	-0.0003	5.00	150.00	1.38
Propeller	4.3207	0.0359	0.1346	5.00	500.00	1.38
Turbine	3.4092	0.4896	0.0030	5.00	150.00	1.38

Pump Data (including electric drives)							
<u>Pump Type</u>	$\mathbf{K}_1$	$\mathbf{K}_2$	$\mathbf{K}_3$	$C_1$	$C_2$	C <sub>3</sub>	$\mathbf{B}_1$
Centrifugal pump	3.3892	0.0536	0.1538	-0.3935	0.3957	-0.00226	1.89
Positive Displacement	3.4771	0.1350	0.14380	-0.24538	0.259016	-0.01363	1.89
Reciprocating pump	3.8696	0.3161	0.12200	-0.2454	0.2590	-0.0136	1.89

Reactor Data						
Reactor Type	$\mathbf{K}_1$	$K_2$	<b>K</b> <sub>3</sub>	$V_{min}(m^3)$	$V_{max}(m^3)$	F <sub>BM</sub>
Autoclave	4.5587	0.2986	0.0020	1.00	15.00	4.0
Fermenter	4.1052	0.5320	-0.0005	0.10	35.00	4.0
Inoculum Tank	3.7957	0.4593	0.0160	0.07	1.00	4.0
Jacketed Agitated	4.1052	0.5320	-0.0005	0.10	35.00	4.0
Jacketed Non-Agitated	3.3496	0.7235	0.0025	5.00	45.00	4.0
Mixer/Settler	4.7116	0.4479	0.0004	0.04	6.00	4.0

Screen Data						
Screen Type	$K_1$	$K_2$	<b>K</b> <sub>3</sub>	$A_{min}(m^2)$	$A_{max}(m^2)$	F <sub>BM</sub>
DSM	3.8050	0.5856	0.2120	0.30	6.00	1.34
Rotary	4.0485	0.1118	0.3260	0.30	15.00	1.34
Stationary	3.8219	1.0368	-0.6050	2.00	11.00	1.34
Vibrating	4.0485	0.1118	0.3260	0.30	15.00	1.34

Tank Data							
Tank Type	$K_1$	$\mathbf{K}_2$	<b>K</b> <sub>3</sub>	$\mathbf{B}_1$	$B_2$	V <sub>min(m3/s)</sub>	V <sub>max(m3/s)</sub>
Fixed Roof	4.8509	-0.3973	0.1445	1.10	0	90	30000
Floating Roof	5.9567	-0.7585	0.1749	1.10	0.00	1000	40000

Turbine Data							
Turbine Type	$\mathbf{K}_1$	<b>K</b> 2	K <sub>3</sub>	FBMCI	FBMCS	<b>Б</b> вмси	Fbmss
Axial	2.7051	1.4398	-0.1776	NA	3.5	NA	6.1
Radial	2.2476	1.4965	-0.1618	NA	3.5	NA	6.1
Vaporizer Data							
Vaporizer Types	$\mathbf{K}_1$	$K_2$	<b>K</b> <sub>3</sub>	V <sub>min(m3)</sub>	V <sub>max(m3)</sub>	P <sub>max(barg)</sub>	$C_1$
Jacketed Vessel	3.8751	0.3328	0.1901	1	100	320	0.1578
		0.0914					
Internal Coil	4.038	2	0.2766	1	100	320	0.1578
		0.0914					
Jacketed Vessel w/ Coil	4.038	2	0.2766	1	100	320	0.1578

	Bare Module Factors, F <sub>BM</sub>									
			GL SS	Glass Lined Ni						
Vaporizer Types	CS	Cu	Coils	Coils	SS	SS Clad	Ni Alloy			
Jacketed Vessel	2.7	3.4	4.7	4.9	4.8	3.8	9.1			

Internal Coil	3.0	3.8	5.2	5.5	5.2	4.1	10.1
Jacketed Vessel w/ Coil	3.0	3.8	5.2	5.5	5.2	4.1	10.1

Evaporator Data									
	Bare Module Factors, $F_{BM}$								
	Cu								
Evaporator Types	CS	Alloy	SS	Ni Alloy	Ti				
Forced Circulation	2.9	3.63	5.08	9.66	14.5				
Falling Film	2.25	2.81	3.94	7.49	11.25				
Agitated (Scraped Wall)	2.25	2.81	3.94	7.49	11.25				
Short Tube	2.9	3.63	5.08	9.66	14.5				
Long Tube	2.9	3.63	5.08	9.66	14.5				

				<u>Horizontal</u>		
				Vessels		
$\mathbf{K}_2$	$\mathbf{K}_3$	$\mathbf{V}_{\min}$	$V_{max}$	$\mathbf{K}_1$	$K_2$	<b>K</b> <sub>3</sub>
0.4485	0.1074	0.3	520	3.5565	0.3776	0.0905
	K <sub>2</sub> 0.4485	K <sub>2</sub> K <sub>3</sub> 0.4485 0.1074	K <sub>2</sub> K <sub>3</sub> V <sub>min</sub> 0.4485 0.1074 0.3	K <sub>2</sub> K <sub>3</sub> V <sub>min</sub> V <sub>max</sub> 0.4485 0.1074 0.3 520	K2         K3         Vmin         Vmax         K1           0.4485         0.1074         0.3         520         3.5565	K2         K3         Vmin         Vmax         K1         K2           0.4485         0.1074         0.3         520         3.5565         0.3776

<u>Vessel Type</u>	B1	B2
Horizontal	1.49	1.52
Vertical	2.25	1.82

#### Materials of Construction

F <sub>M CS</sub>	1.0
$F_{M SS clad}$	1.7
F <sub>M SS</sub>	3.1
$F_{M Ni \ clad}$	3.6
$F_{M Ni}$	7.1

F <sub>M Ti clad</sub>	4.7
F <sub>M Ti</sub>	9.4

Tower Trays					
<u>Tray Type</u>	$K_1$	$K_2$	<b>K</b> <sub>3</sub>	$A_{min}(m^2)$	$A_{max}(m^2)$
Sieve	2.9949	0.4465	0.3961	0.07	12.3
Valve	3.3322	0.4838	0.3434	0.7	10.5
Demister	3.2353	0.4838	0.3434	0.7	10.5
$F_{BM}$					
MOC		Sieve	Valve	Demister	
CS		1.0	1		
SS		1.8	1.83	1.0	
Fluorocarbon				1.8	
Ni-alloy		5.6	5.58	5.6	

 $Fq = 10^{0.4771+0.08516} \text{ Log N } -0.3473 \text{ [Log N]}^2$ 





Ceramic	3.0664	0.9744	0.0055	0.03 62	8 4.14
304 SS	3.2999	0.9744	0.0055	0.03 62	8 7.09
Plastic Saddle	2.4493	0.9744	0.0055	0.03 62	8 1.00

#### Utilities Summary

Name	Total Module Cost	Grass Roots Cost	Utility Used	Efficiency	Actual Usage	Annual Utility Cost
E-	\$	\$	Medium-		14400	\$
101	151,565	216,000	Pressure		MJ/h	-
E-	\$	\$	Low-		2030 MJ/h	\$
102	156,000	222,000	Pressure Steam			-
E-	\$	\$	Medium-		12400	\$
103	199,000	283,000	Pressure Steam		MJ/h	1,467,000
E-	\$	\$	Medium-		2490 MJ/h	\$
104	141,000	201,000	Pressure Steam			-
E-	\$	\$	Medium-		3140 MJ/h	\$
105	155,000	220,000	Pressure Steam			-
E-	\$	\$	Medium-		5790 MJ/h	\$
106	99,000	141,000	Pressure Steam			-
E-	\$	\$	Medium-		5670 MJ/h	\$
107	110,000	156,000	Pressure Steam			-

Figure 6-2 Utilities Summary

## **Utility Summary**

Classification	Price (\$/kg)		Flowrate (kg/h)	Annual Cost		
Raw Material	\$	-	5853.00	\$	-	
Raw Material	\$	1.50	3520.00	\$	43,940,160	
Product	\$	(0.19)	720.00	\$	(1,138,450)	
Product	\$	(12.00)	718.00	\$	(71,702,352)	
Product	\$	(10.00)	4009.76	\$	(333,692,227)	
Raw Material	\$	10.00	1193.60	\$	99,331,392	
Raw Material	\$	9.00	1264.00	\$	94,671,072	
	Classification Raw Material Raw Material Product Product Product Raw Material Raw Material	ClassificationPriRaw Material\$Raw Material\$Product\$Product\$Product\$Raw Material\$Raw Material\$	ClassificationPrice (\$/kg)Raw Material\$ -Raw Material\$ 1.50Product\$ (0.19)Product\$ (12.00)Product\$ (10.00)Raw Material\$ 10.00Raw Material\$ 9.00	Classification         Price (\$/kg)         Flowrate (kg/h)           Raw Material         \$ -         5853.00           Raw Material         \$ 1.50         3520.00           Product         \$ (0.19)         720.00           Product         \$ (12.00)         718.00           Product         \$ (10.00)         4009.76           Raw Material         \$ 10.00         1193.60           Raw Material         \$ 9.00         1264.00	Classification         Price (\$/kg)         Flowrate (kg/h)         A           Raw Material         \$         -         5853.00         \$           Raw Material         \$         1.50         3520.00         \$           Product         \$         (0.19)         720.00         \$           Product         \$         (12.00)         718.00         \$           Product         \$         (10.00)         4009.76         \$           Raw Material         \$         10.00         1193.60         \$           Raw Material         \$         9.00         1264.00         \$	

## Cash Flow Diagram



Figure 6-3 Cash Flow Diagram

# Chapter 07

## 7 Result and Discussion

Natural gas has emerged as a potential substrate for the synthesis of minerals and energy in electricity and manufacturing. This substance can be utilized in various types of power generating, transportation fuel, and residential space heating. The aim of this study is to establish system that syntheses, modelling, and integrating methodologies for a shales gases - to-Di Methyl ether plant using both, directly and indirectly. The price of CH3OH and shale gas are by far the most critical elements determining the costs of an oil and gas company.

Nowadays, the calculation of aeroplane dimensions by a couple of guidance systems is expected to be the main stand-by marketing strategies on boarding a civil aeroplane. However, the outcome of the research show low evidence for the placement of the aircraft by a global DME transmitter infrastructure. DME Connectivity is constrained in a number of places, particularly Northern Asia, Central Africa, Southeast Asia and Western Australia. The installation of navigation systems can be viewed as a stand-by strategy solely on the european side within the anticipated provider network. In order to guarantee the additional strength of air safety around the world, the scope and effectiveness of the wide network for guidance tool should be greatly expanded. In the DME's steam reform, the influence of temperature, pressures and water to a carbon was demonstrated to be significant.

The estimation is based on a process flow diagram, utility balance, and P&ID. In this estimation, the exact sizing of equipment that is used in study estimate is essential. The final estimation requires preliminary specification of all chemical equipment, instrumentation, utilities and off-site. The level of accuracy of the estimate is depending upon: Effort and Time

available Cost Revenue Estimator Vs Cost of Making Size of DME plant. There are several people and records that are the best Source for estimating information.

The engineer must know the factor that affects the price of the product. The company policies depend on labour unions because there is an effect of labour charge overtime work and the operator and engineer that work in a company in overtime work. There is a direct effect on the cost of industrial processes due to governmental regulations and rules. All industry, engineering and construction news indexes for the year from 1926 to 1990 are shown in red. In this article, we study the 3D diagram of chemical processes.

We also looked at the structural design and building of chemical plant. We conclude by looking at the economic analysis of large equipment used in DME process. In the last chapter, we examine the rate of cost improvement in chemical technology. The learning phenomena are not factor that promote the relationship between declined cost unit and cumulative production. There are four hypotheses that are regarding relationship between cost improvement and technical characterizes.

The higher level of complexity are cause high improvement. Higher the capital investment is causes rapid improvement in chemical process because process will provide less value of performance and it also cause less cost improvement. There is relationship between learning curve and technological innovation and economical scale. There are 37 chemical process and products that are factor associated with cost improvement. The higher level of R&D is causes more rapid cost improvement, according to the study. In this research work, it has been found that there is no relationship between "scaling factor" and cost improvement for technological analysis. Cost improvement slope is based on chemical processes in database. The price

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change in feedstock are causes big effect on prices on product. In the first hypotheses there are relationship between cost improvement and industrial management for the chemical process. The second hypothesis is on management information transfer and organization of rapid improvement cost. There is magnitude of relationship between R&D expenditure and cost improvement has very important implication of industrial competitiveness. We have hoped to test relationship between different R&d expenditure on refinement of different processes by using different multiple regression model.

Combinatorial effects of aspects on the rate of return of distinct chemical species were clarified in the liquid phase. The primary motivation of this work are the construction of all organic compound models predictor for the steam reformation of DME. Statistical significance was demonstrated for all of the models developed. These conclusions have a number of practical ramifications. They can make quick predictions based on a known set of process inputs because they have the necessary resources. It can also act as a basis for various techniques to optimizing. These associations will enable early estimations of production line and product selective during the design phase of the DME reform. This will of course change the outcome between available options in many aspects.

## Conclusion

This research work is on "Process Design and Simulation of DME Production" is my own work. This work is not doing anyone before, or nothing has published a research paper. The data that has been used in this research paper appropriately referred. Natural gas has emerged as a potential substrate for the synthesis of minerals and energy in electricity and manufacturing. This substance can be utilized in various types of power generating, transportation fuel, and residential space heating. The aim of this research is to establish system syntheses, modelling, and integrating methodologies for a shalesgas-to-DiMethyl ether plant. The demand for worldwide energy is continuously growing. 82 percent of the energy needs of the United States are generated from fossil fuels. The direct approach is more cost-effective than that of the inductive channel from an economic perspective. Squeeze research was employed in order to complete the heat incorporation of the system.

It was possible to synthesize the internal and external process voidable contract by utilizing six and ten key processing phases. Natural gas restricts its significance in the upcoming projects of the energy world. In the, 84 percent of natural gas is produced, which makes it environmentally friendly. More advanced technologies than traditional methods are needed for the manufacturing of gas from shale sources. Shale gas has the cleanest combustion and has the largest share in the new resources strategy to supply energy needs. DME is the lightest, completely non-dangerous and non-toxic ether. It possesses physiological qualities comparable to those of LPG. DME can be stored and supplied with minimal change by utilizing current infrastructures and technologies. This is used as a substitute for LPG in cookery and thermal applications and an aerosols propulsion in paint and other aerosols products. The majority of

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DMEs currently on the market are produced in developed countries.

There are also new contenders for capability development, such as Ethiopia, Russia, Libya, Iran and Tashkent. DME is the gasoline that is ecologically responsible, and that is its benefit over the other hydrocarbons. By ingesting the greatest possible values, the WTT efficiency of crude oil powers can be increased to over Ninety percent. WTT of DME, on the other hand, is somewhat more than 70% [23]. When compared to fossil fuels and GTL, DME emits the least amount of pollution at low loads. The Gas – to – liquids strategy requires the reformation of regular gas to produce biogas (also known as syngas). In picking reform styles or types, the following key concepts should be considered: process goals, material availability, oil reserves, final product, storage capacity, climate, and structural problems In particular, there are four types of reform: partly oxidizing, steaming restructure, dryness restructure, and mixtures of these modifications (as well as other variations).

The results of this investigation demonstrate both the possibilities and the difficulties of the extraction procedure. It is necessary to combine burning with water electrolysis in order to achieve the required H2:CO ratio in heat cracking reformation of CH4. Most commonly used catalysts in reforming processes include supporting metal, chromium and ferrous catalysis, supporting metal oxide hydrocarbons, and metal oxide carbide catalysis. It was developed by Franz Fischers and Hens Tropschs, who designed the first commercial reactors in 1935. Aspen plus has increased the DME productionup to 6%. we are used Peng-Robison method in Aspen plus software. We have done pinch analysis to increase the efficiency of heat recovery up to 14%. After the optimization we have done cost analysis to check the profit of the systems.

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